



US008170088B2

(12) **United States Patent**
Martin

(10) **Patent No.:** **US 8,170,088 B2**
(45) **Date of Patent:** ***May 1, 2012**

(54) **METHODS FOR DETERMINING A REFERENCE SIGNAL AT ANY LOCATION ALONG A TRANSMISSION MEDIA**

FOREIGN PATENT DOCUMENTS
EP 0959522 A1 11/1999
(Continued)

(75) Inventor: **G. Patrick Martin**, Merritt Island, FL (US)

OTHER PUBLICATIONS

(73) Assignee: **Harris Corporation**, Melbourne, FL (US)

Vavrda, M., "Digital Beamforming in Wireless Communications" Institute of Radio Electronics, Faculty of Electrical Engineering of Technology; Brno Univ. of Technology, Purkynova 118, Czech Republic; downloaded from the internet on Oct. 13, 2010 at <<http://www.urel.feec.vutbr.cz/ra2007/archive/ra2004/abstracts/110.pdf>>.

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 809 days.

This patent is subject to a terminal disclaimer.

(Continued)

(21) Appl. No.: **12/273,797**

Primary Examiner — Juan A Torres

(22) Filed: **Nov. 19, 2008**

(74) Attorney, Agent, or Firm — Fox Rothschild, LLP; Robert J. Sacco

(65) **Prior Publication Data**
US 2010/0124302 A1 May 20, 2010

(57) **ABSTRACT**

(51) **Int. Cl.**
H04B 3/46 (2006.01)
(52) **U.S. Cl.** **375/224**
(58) **Field of Classification Search** **375/224**
See application file for complete search history.

Methods (200, 300) for determining a reference signal (V_{ref}). The methods involve (202, 204, 302, 304) sensing at a first location along the transmission media (108, 502) a first signal (V_f) propagated thereover in a forward direction and a second signal (V_r) propagated thereover in a reverse direction opposed from the forward direction. The second signal being a reflected version of the first signal. A sum signal (S) is determined (206, 306) by adding the first and second signals together. A difference signal (D) is determined (208, 308) by subtracting the second signal from the first signal. Thereafter, a first exponentiation signal (E_s) is determined (210, 310) using S. A second exponentiation signal (E_D) is determined (212, 312) using D. The first exponentiation signal is subtracted (214, 314) from the second exponentiation signal to obtain a reference signal (V_{ref}). V_{ref} can be determined at any location along the transmission media. V_{ref} can be used to control the phases and/or amplitudes of communication signals.

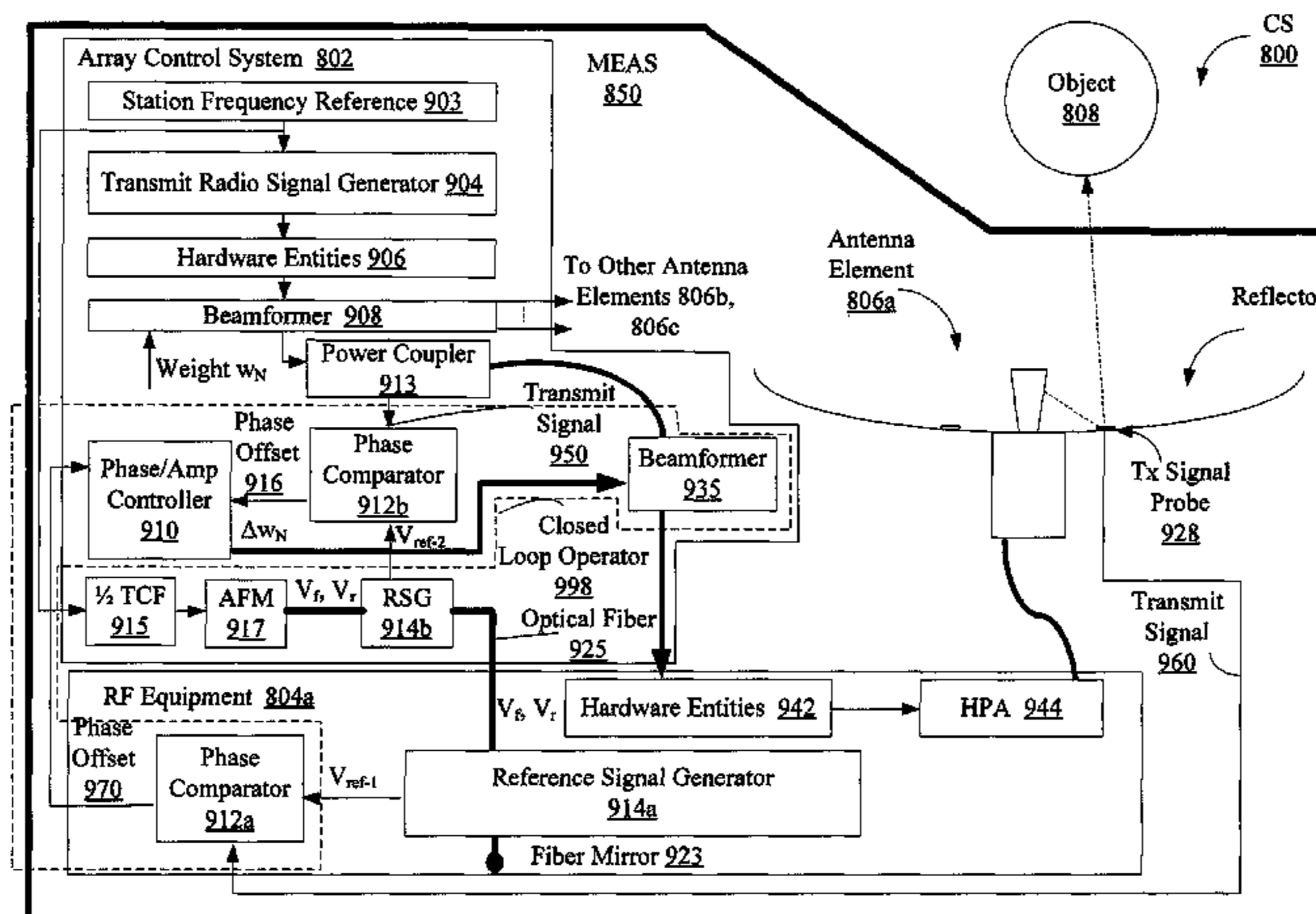
(56) **References Cited**

U.S. PATENT DOCUMENTS

3,646,558	A	2/1972	Campanella	
3,697,997	A	10/1972	Cooper	
3,961,172	A	6/1976	Hutcheon	
4,060,809	A	11/1977	Baghdady	
4,358,822	A	11/1982	Sanchez	
4,532,518	A	7/1985	Gaglione et al.	
4,843,397	A	6/1989	Galati et al.	
4,862,180	A	8/1989	Martin	
5,008,680	A	4/1991	Willey et al.	
5,157,404	A	10/1992	Rowe et al.	
5,227,736	A *	7/1993	Tucker et al.	330/149

(Continued)

20 Claims, 10 Drawing Sheets



U.S. PATENT DOCUMENTS

5,313,308	A	5/1994	Hasegawa et al.	
5,541,607	A	7/1996	Reinhardt	
5,629,709	A	5/1997	Yamashita	
5,698,848	A *	12/1997	Belk	250/227.11
5,742,253	A	4/1998	Conroy et al.	
5,805,983	A	9/1998	Naidu et al.	
5,990,721	A	11/1999	Mellitz	
6,002,360	A	12/1999	Wolcott et al.	
6,075,484	A *	6/2000	Daniel et al.	342/372
6,199,032	B1	3/2001	Anderson	
6,275,091	B1 *	8/2001	Saeki	327/396
6,377,119	B1 *	4/2002	Hays	330/149
6,434,435	B1	8/2002	Tubel et al.	
6,480,153	B1	11/2002	Jung et al.	
6,563,358	B1	5/2003	Goulette	
6,597,730	B1	7/2003	Bader	
6,611,537	B1 *	8/2003	Edens et al.	370/503
6,647,506	B1	11/2003	Yang et al.	
6,806,837	B1	10/2004	Saucier et al.	
6,816,822	B1	11/2004	Hess et al.	
6,826,521	B1	11/2004	Hess et al.	
6,834,180	B1	12/2004	Marshall	
6,861,975	B1	3/2005	Coleman, Jr. et al.	
6,862,514	B2	3/2005	Ehara	
6,897,807	B2	5/2005	Kishigami et al.	
6,975,268	B2 *	12/2005	Coleman et al.	342/375
7,057,555	B2	6/2006	Lewis	
7,230,970	B1 *	6/2007	Bryant	375/130
7,366,248	B2	4/2008	Wang et al.	
7,460,067	B2	12/2008	Allen et al.	
7,570,686	B2 *	8/2009	Krinsky et al.	375/222
7,663,542	B1	2/2010	Goodzeit et al.	
7,705,779	B2	4/2010	Goldberg et al.	
7,742,904	B2	6/2010	Healy et al.	
7,773,666	B2 *	8/2010	Belge et al.	375/222
7,852,910	B2 *	12/2010	Belge	375/222
7,969,358	B2	6/2011	Martin et al.	
2002/0123045	A1	9/2002	Martinell et al.	
2002/0196186	A1	12/2002	Holt	
2003/0236081	A1	12/2003	Braun	
2004/0169602	A1	9/2004	Hamada et al.	
2006/0109927	A1	5/2006	Magee et al.	
2007/0078530	A1	4/2007	Blevins et al.	
2007/0165691	A1 *	7/2007	Taverner et al.	374/120
2007/0168057	A1	7/2007	Blevins et al.	
2008/0129613	A1	6/2008	Ermutlu et al.	
2009/0048748	A1	2/2009	Zhao et al.	
2009/0167607	A1	7/2009	Holder	
2009/0315565	A1 *	12/2009	Wyar et al.	324/533
2010/0123618	A1 *	5/2010	Martin et al.	342/174
2010/0123624	A1	5/2010	Miner et al.	
2010/0124263	A1	5/2010	Martin et al.	
2010/0124625	A1	5/2010	Blair	
2010/0124895	A1	5/2010	Martin et al.	
2010/0125347	A1	5/2010	Martin et al.	
2011/0022375	A1	1/2011	Odille et al.	

FOREIGN PATENT DOCUMENTS

EP	1271802	A1	1/2003
JP	2004 147130		5/2004
WO	WO-01 65637	A2	9/2001
WO	WO-2007001252	A1	1/2007
WO	WO-2008074925	A1	6/2008

OTHER PUBLICATIONS

Haynes, T., White Paper, "A Primer on Digital Beamforming", Spectrum Signal Processing, Mar. 26, 1998.

Krim, H., et al. "Two Decades of Array Signal Processing Research", IEEE Signal Processing Magazine, pp. 67-94; Jul. 1996.

Swarup, G., et al., "Phase Adjustment of Large Antennas" IRE Transactions on Antennas and Propagation, IEEE, USA, vol. 10, No. 1., Jan. 1, 1961, pp. 75-81.

Hills, et al., "The Atacama Large Millimeter/submillimeter Array", Proc. of SPIE vol. 7012, 70120N (2008) SPIE, PO Box 10 Bellingham WA 98227-0010 USA, Jul. 10, 2008, XP040439602, abstract.

Steinberg, Bernard D., "Phase Synchronizing a Nonrigid, Distributed, Transmit-Receive Radar Antenna Array", IEEE Transactions on Aerospace and Electronic Systems, IEEE Service Center, Piscataway, NJ, US, vol. AES-10, No. 5, Sep. 1, 1982, pp. 609-620, XP011166973, ISSN: 0018:9251.

Bourgeois, et al., "Computer antenna pointing for orbital debris radar", Antennas and Propagation Society International Symposium, 1993, vol. 2, pp. 758-176.

Written Opinion of the International Preliminary Examining Authority, mailed Dec. 1, 2010, issued in application serial No. PCT/US2009/064973 in the name of Harris Corporation.

International Search Report and Written Opinion mailed Feb. 9, 2010, in connection with application serial No. PCT/US2009/065092, in the name of Harris Corporation.

International Search Report and Written Opinion mailed Feb. 9, 2010, in connection with application serial No. PCT/US2009/064973, in the name of Harris Corporation.

International Search Report mailed May 20, 2010; International Application Serial No. PCT/US2009/064942, in the name of Harris Corporation.

International Search Report mailed May 20, 2010; International Application Serial No. PCT/US2009/065029, in the name of Harris Corporation.

International Search Report mailed May 20, 2010; International Application Serial No. PCT/US2009/065039, in the name of Harris Corporation.

International Search Report mailed Mar. 4, 2010; International Application Serial PCT/US2009/065066, in the name of Harris Corporation.

Li, Y., et al., "Adaptive Blind Source Separation and Equalization for Multiple-Input/Multiple-Output Systems" IEEE Transactions on Information Theory, vol. 44, No. 7, Nov. 2, 1998, pp. 2864-2876, XP002576178.

Qin, J. S et al: "A survey of industrial model predictive control technology" Control Engineering Practice, Pergamon Press, Oxford, GB, vol. 11, Jan. 1, 2003, pp. 733-764, XP002435295 ISSN: 0967-0661.

Gawronski, W.: "Control and Pointing Challenges of Large Antennas and Telescopes" IEEE Transactions on Control Systems Technology, IEEE Service Center, New York, NY, US, vol. 15, No. 2, Mar. 1, 2007, pp. 276-289, XP011168299 ISSN: 1063-6536.

Maneri E et al: "LOG controller design using GUI: Application to antennas and radio-telescopes" ISA Transactions, Instrument Society of America. Pittsburgh, US, vol. 39, No. 2, Apr. 1, 2000, pp. 243-264, XP004313422.

* cited by examiner

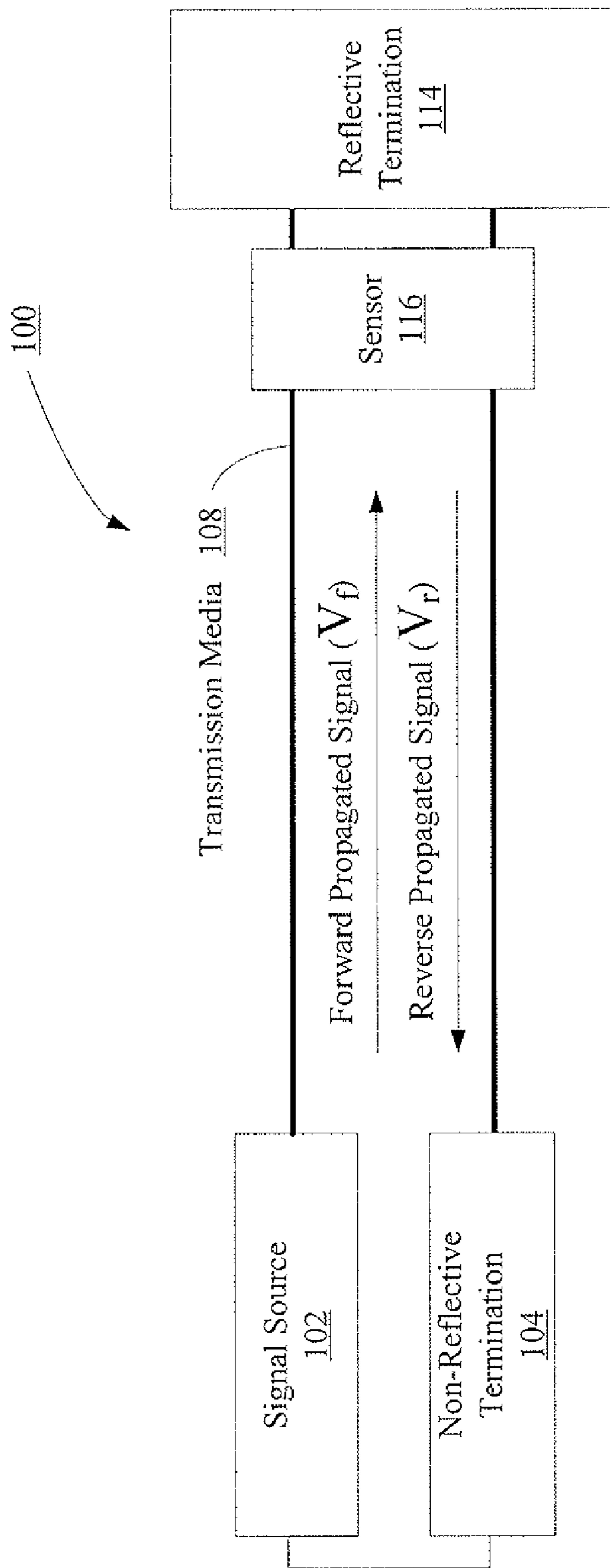
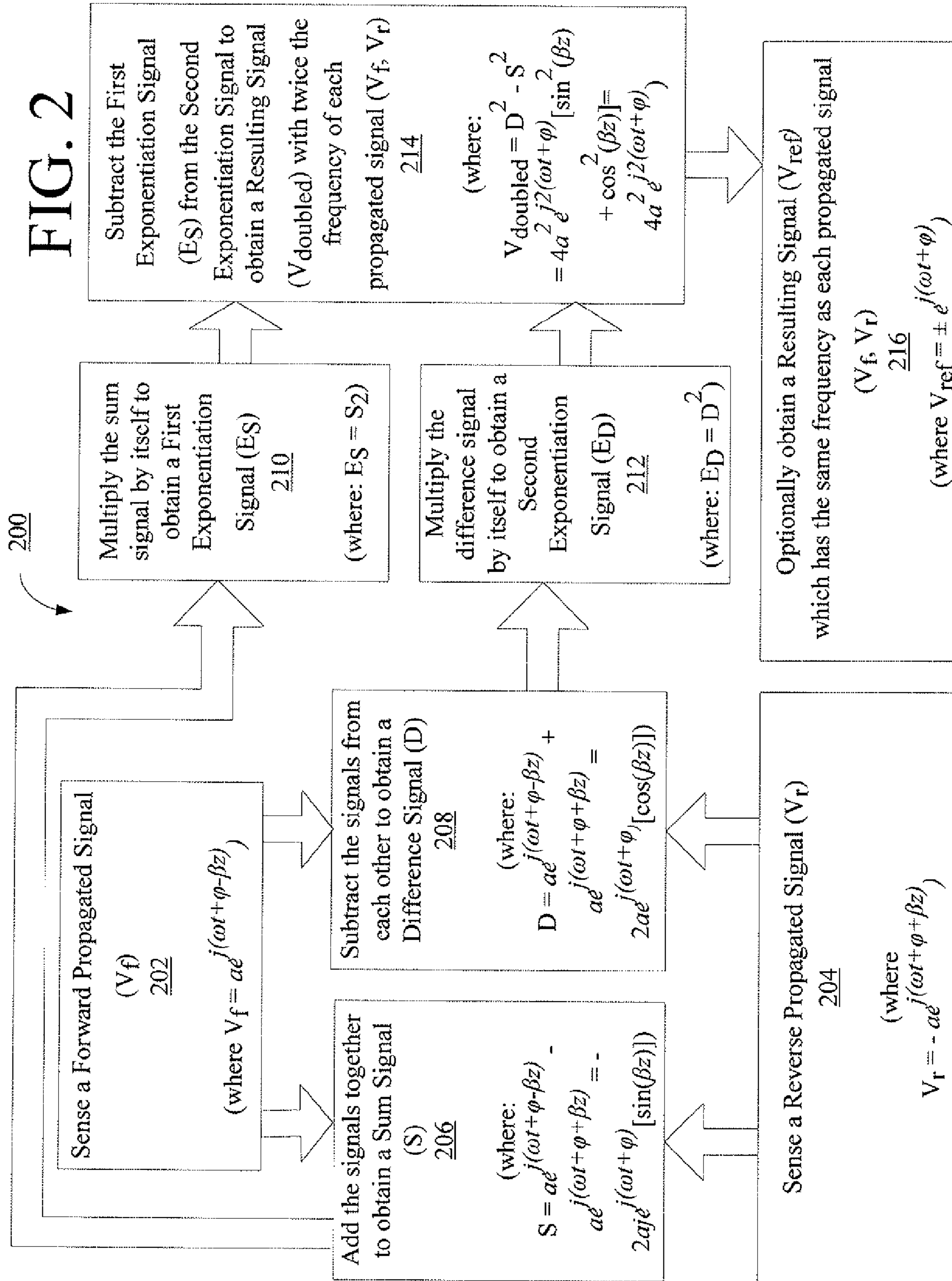


FIG. 1

FIG. 2



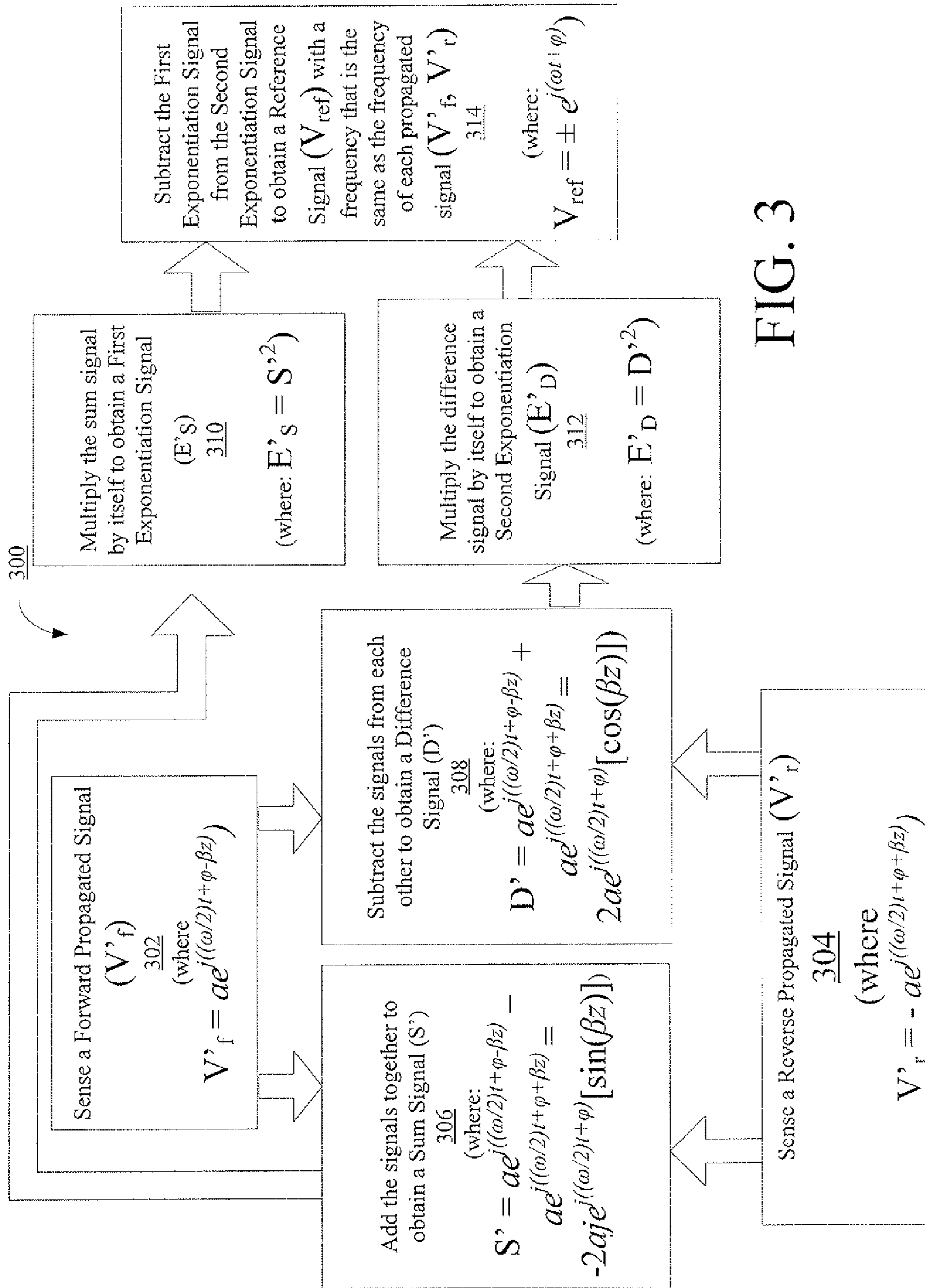


FIG. 3

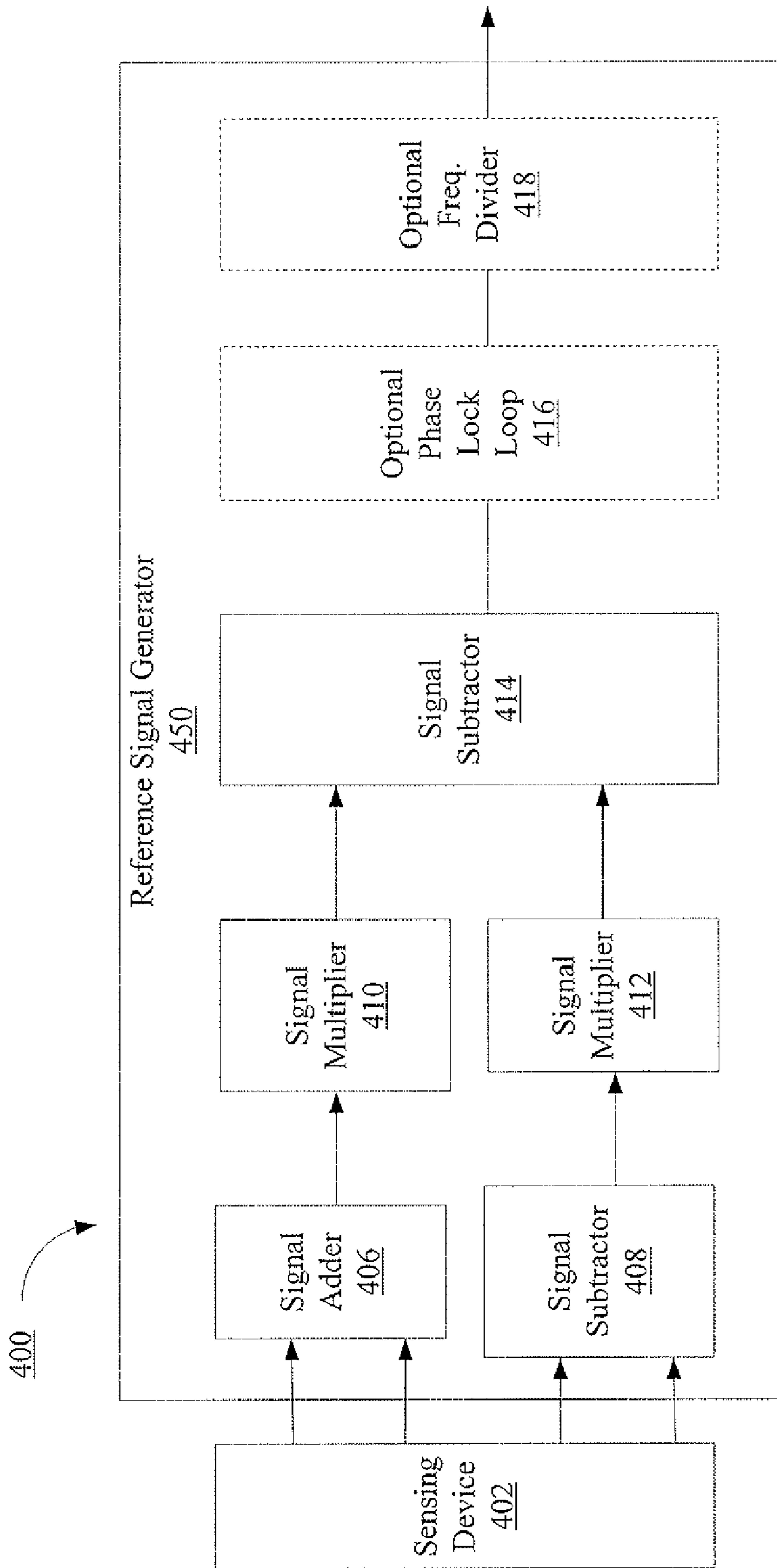


FIG. 4

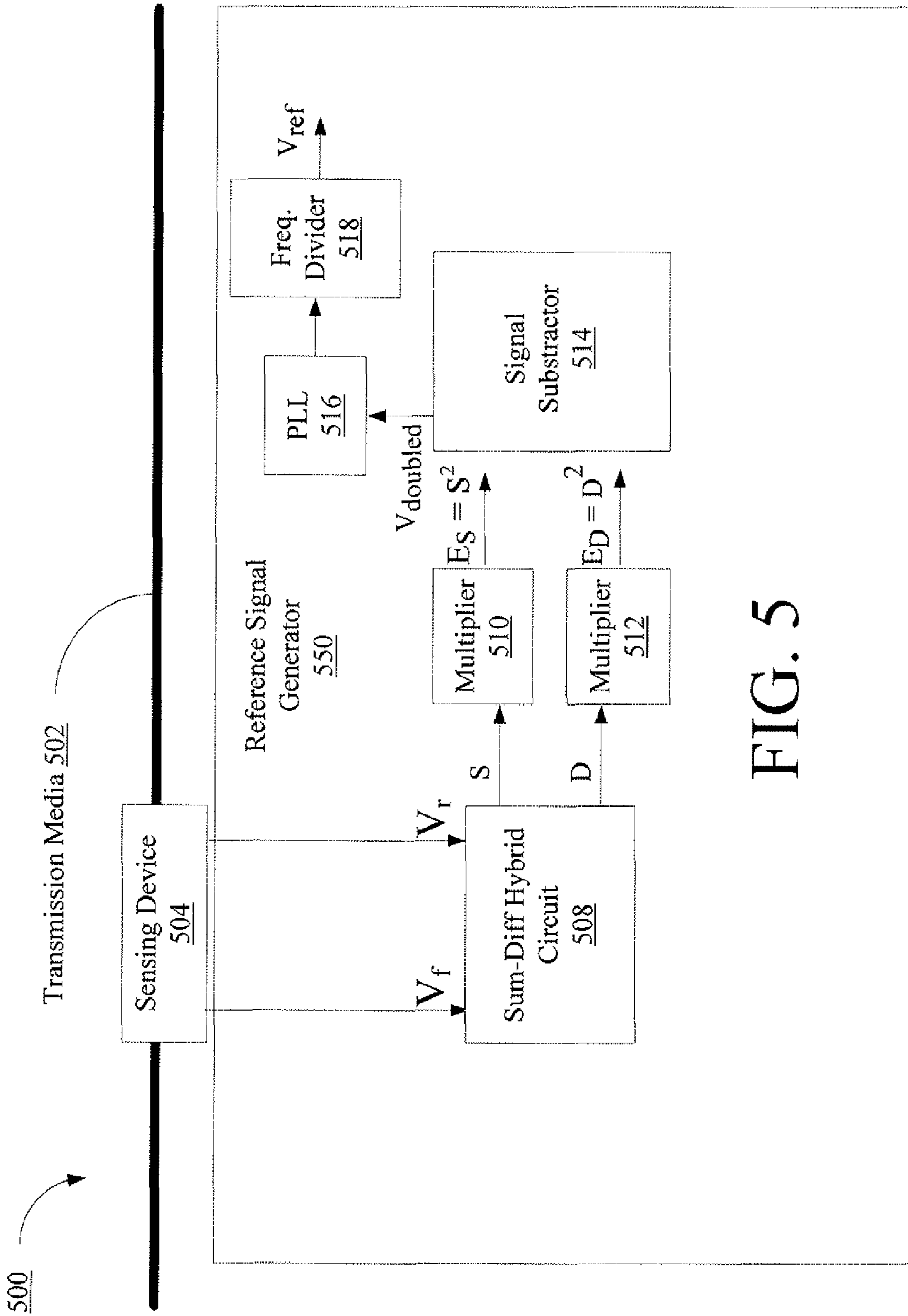
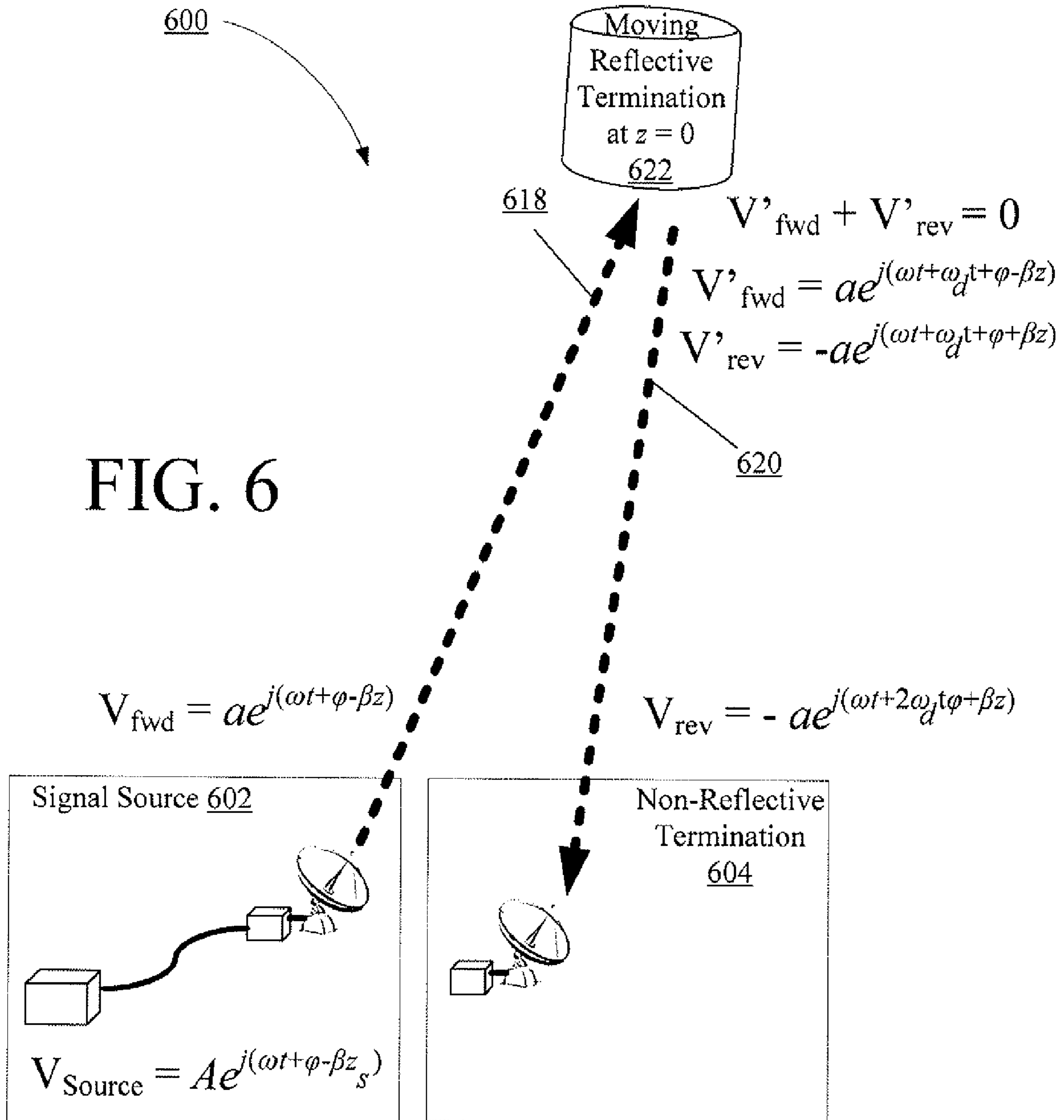
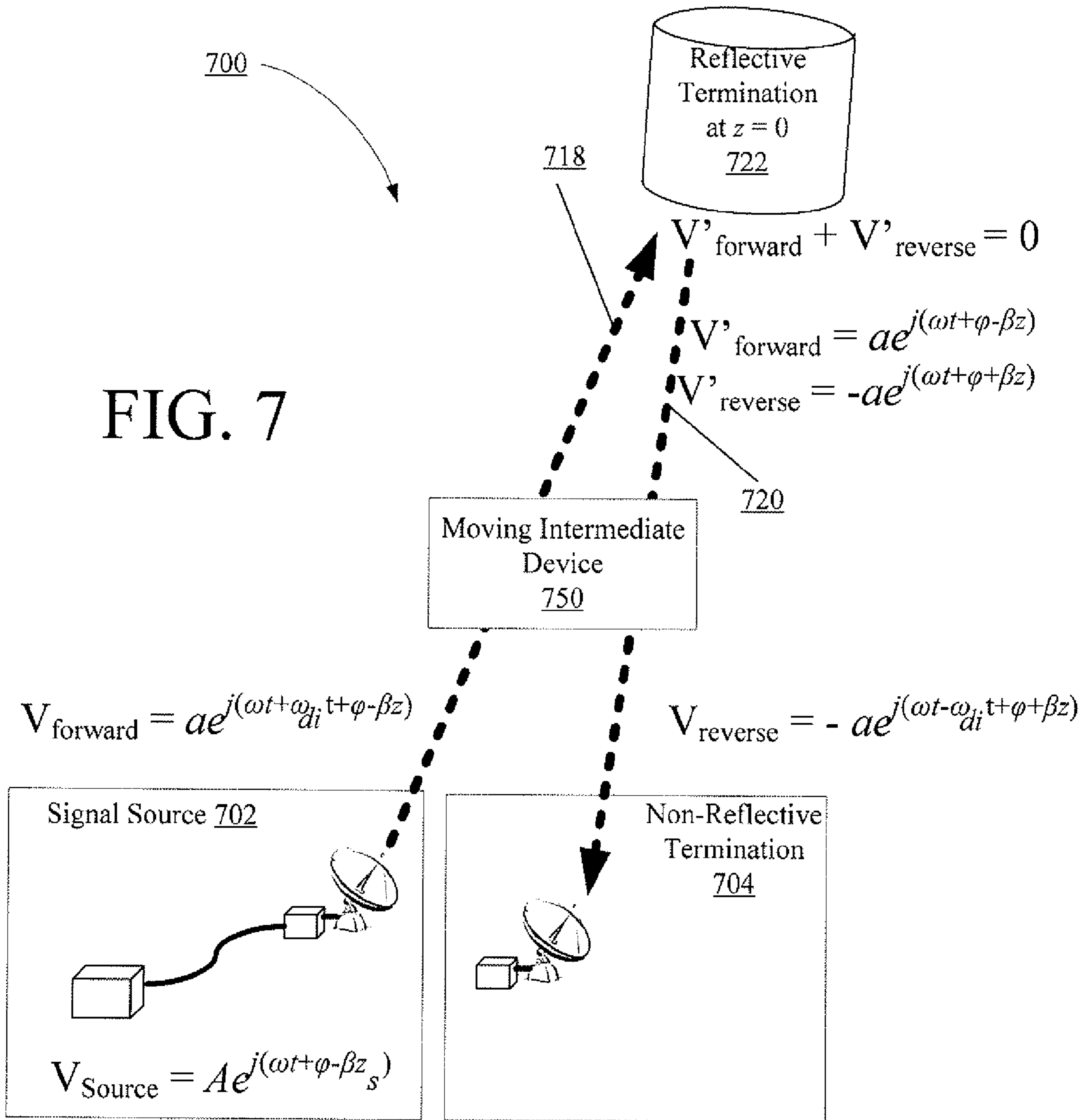


FIG. 5





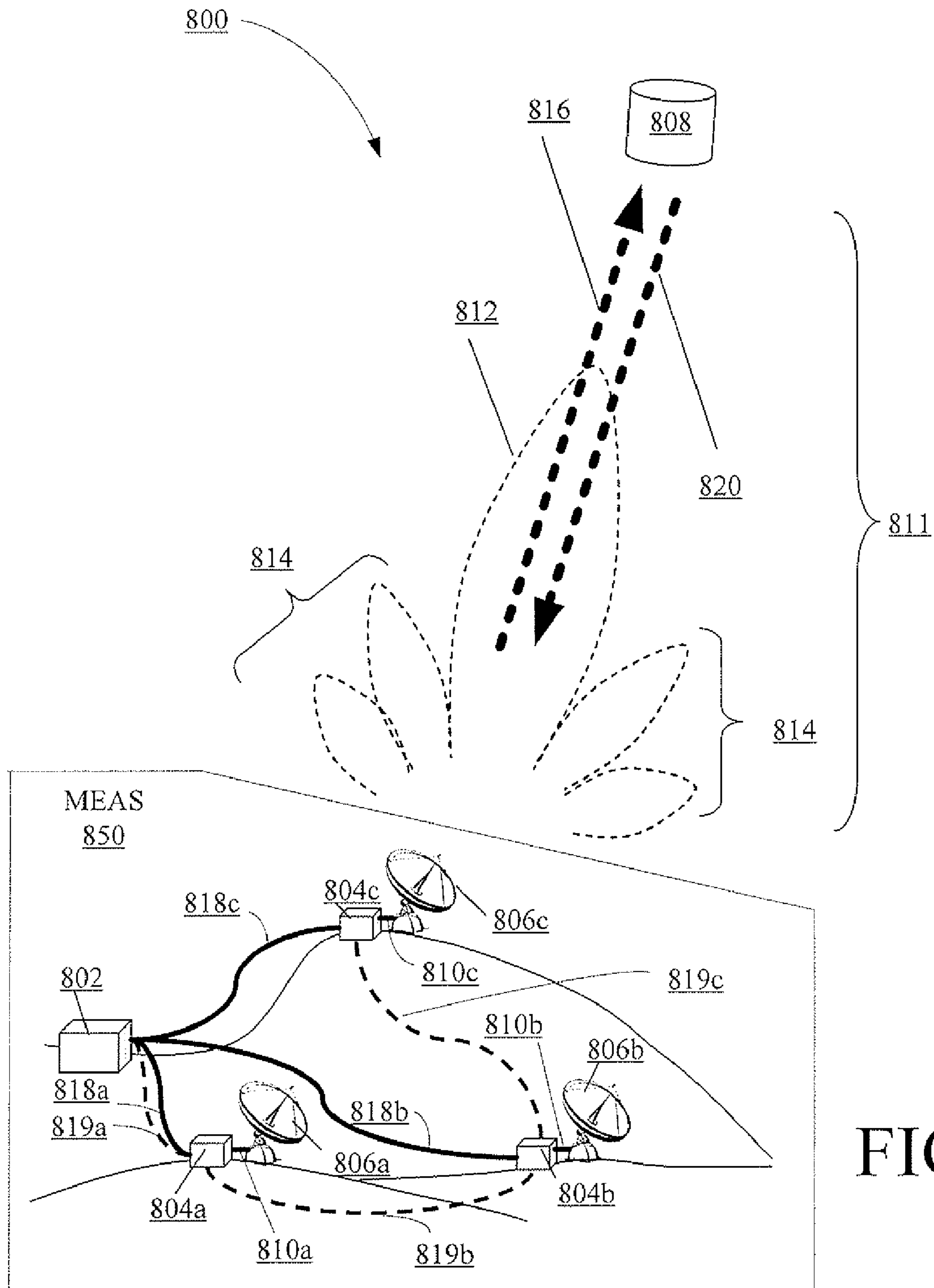


FIG. 8

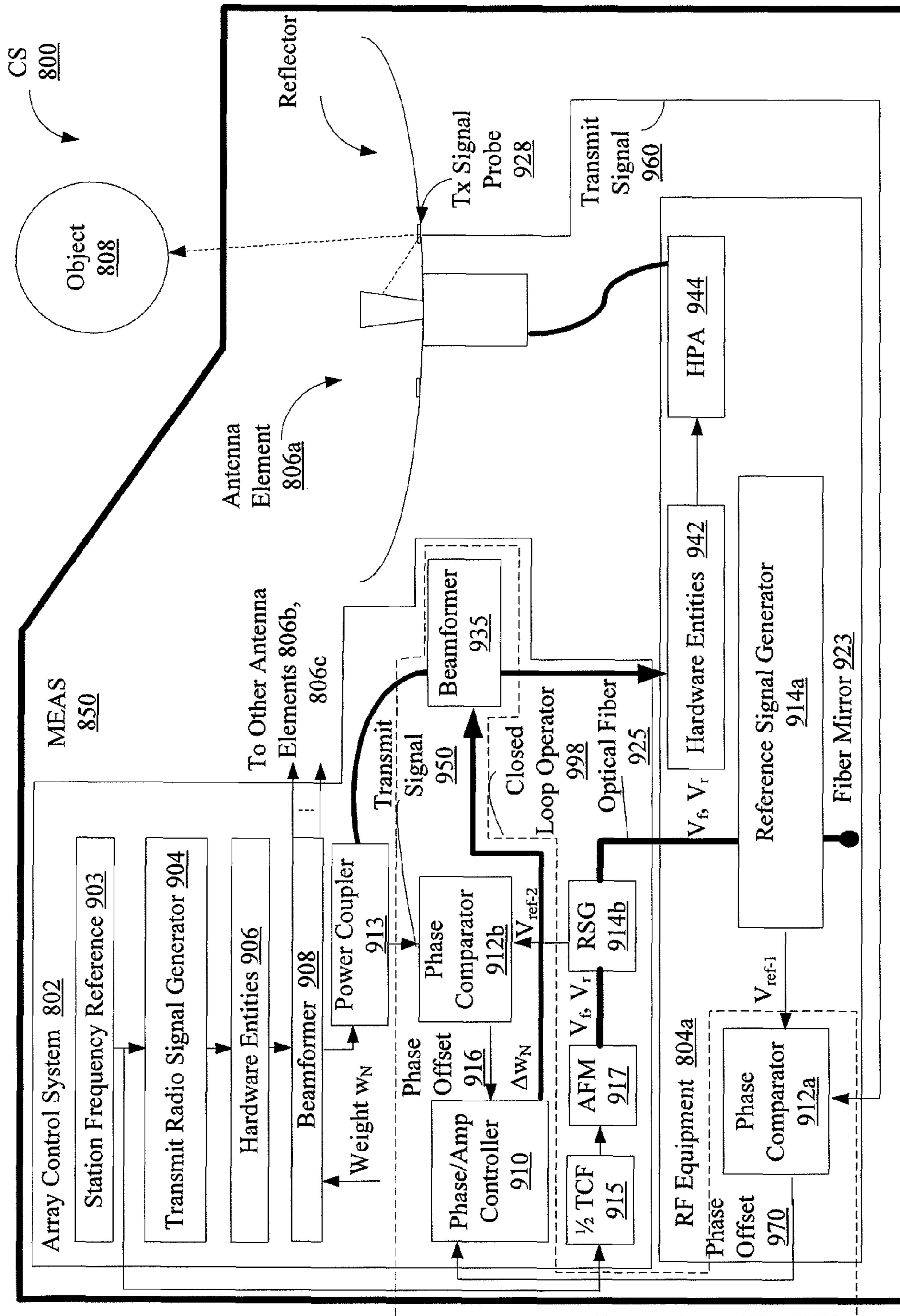


FIG. 9

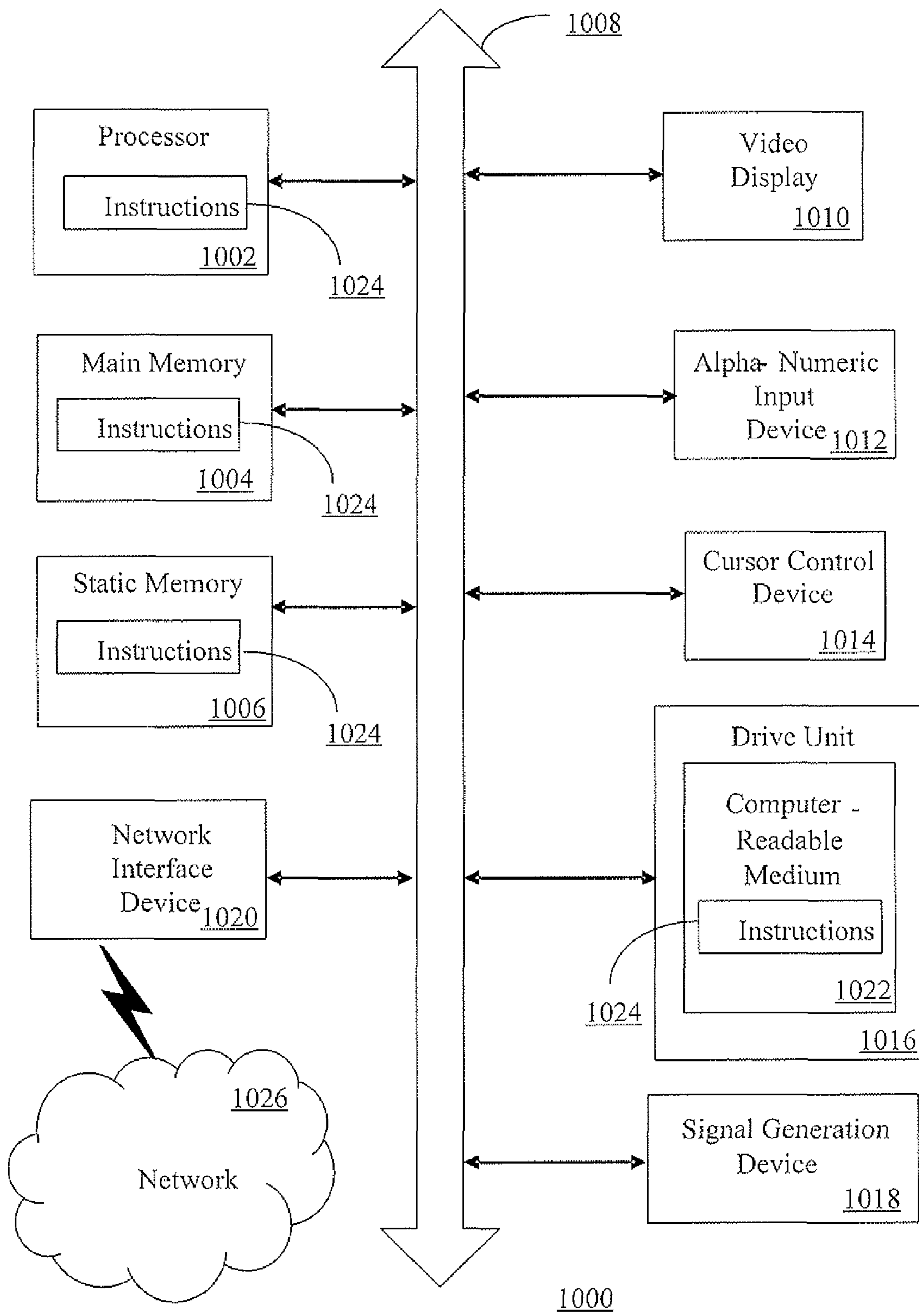


FIG. 10

1

**METHODS FOR DETERMINING A
REFERENCE SIGNAL AT ANY LOCATION
ALONG A TRANSMISSION MEDIA**

BACKGROUND OF THE INVENTION

1. Statement of the Technical Field

The invention concerns systems implementing methods for determining a reference signal at any location along a transmission media.

2. Description of the Related Art

There are many systems and applications known to those having ordinary skill in the art that can benefit from an ability to determine a reference signal at any location along a transmission media. Such systems include, but are not limited to, radar systems and communication systems. For example, a conventional wireless communication system typically includes a system controller, a plurality of antenna controllers, and a plurality of antenna elements (e.g., a plurality of dish antennas). Each of the antenna elements is communicatively coupled to the system controller and a respective one of the antenna controllers via a cable assembly. During transmission and reception, each antenna element converts electrical signals into electromagnetic waves, and vice versa. The phases of the signals to be transmitted from and received by the antenna elements can be shifted as a result of environmental effects on hardware components of the system controller, hardware components of the antenna controllers, and the cable assemblies connecting the antenna elements to the controllers. These phase shifts typically result in the steering of the radiated main beam in the wrong direction. In order to overcome the various limitations of the communication system, it needs to implement a beamforming solution that counter acts the phase shifts resulting from environmental effects on the hardware components and cables thereof.

SUMMARY OF THE INVENTION

Embodiments of the present invention concern methods for determining at least one reference signal. The method embodiments involve sensing at a first location along the transmission media a first signal propagated over the transmission media in a forward direction and a second signal propagated over the transmission media in a reverse direction opposed from the forward direction. The transmission media can include, but is not limited to, free space, waveguides, coaxial transmission lines, optical fibers, and acoustic media. The second signal is a reflected version of the first signal. Thereafter, a first sum signal is determined by adding the first and second signals together. Similarly, a first difference signal is determined by subtracting the second signal from the first signal. A first exponentiation signal is then determined using the first sum signal. Likewise, a second exponentiation signal is determined using the first difference signal. The first exponentiation signal is subtracted from the second exponentiation signal to obtain a first reference signal. Notably, the first reference signal can be subsequently utilized by a communication system to control the phase of a communication signal.

According to an aspect of the present invention, the first reference signal can have a first frequency equal to a second frequency of the first signal. Alternatively, the first reference signal can have a first frequency different than a second frequency of the first signal. In such a scenario, the first reference signal can be processed to obtain an adjusted reference signal with a third frequency equal to the second frequency of the first signal.

2

According to another aspect of the present invention, the method embodiments can further involve sensing at a second location different from the first location along the transmission media the first and second signal. Thereafter, a second reference signal is determined using the first and second signal sensed at the second location. The second reference signal has the same phase as the first reference signal.

The second reference signal is determined by determining a second sum signal by adding the first and second signals sensed at the second location together and a second difference signal by subtracting the second signal sensed at the second location from the first signal sensed at the second location. The second reference signal is also determined by determining a third exponentiation signal using the second sum signal and a fourth exponentiation signal using the second difference signal. The third exponentiation signal is subtracted from the fourth exponentiation signal to obtain the second reference signal.

BRIEF DESCRIPTION OF THE DRAWINGS

Embodiments will be described with reference to the following drawing figures, in which like numerals represent like items throughout the figures, and in which:

FIG. 1 is a block diagram of an exemplary system including a stationary reflective termination that is useful for understanding the present invention.

FIG. 2 is a conceptual diagram of a first exemplary method (or process) for determining a reference signal at any location along a transmission media.

FIG. 3 is a conceptual diagram of a second exemplary method (or process) for determining a reference signal at any location along a transmission media.

FIG. 4 is a block diagram of a first exemplary embodiment of a system configured to generate a reference signal in accordance with the methods of FIGS. 2 and 3.

FIG. 5 is a block diagram of a second exemplary embodiment of a system configured to generate a reference signal in accordance with the method of FIG. 2.

FIG. 6 is a block diagram of an exemplary system including a moving reflective termination that is configured for determining a reference signal.

FIG. 7 is a block diagram of an exemplary system including a moving intermediate device that is configured for determining a reference signal.

FIG. 8 is a block diagram of a communication system configured to generate reference signals.

FIG. 9 is more detailed block diagram of the communication system of FIG. 8.

FIG. 10 is a schematic view of a computer system within which a set of instructions operate according to an embodiment of the present invention.

DETAILED DESCRIPTION

The present invention is described with reference to the attached figures, wherein like reference numbers are used throughout the figures to designate similar or equivalent elements. The figures are not drawn to scale and they are provided merely to illustrate the instant invention. Several aspects of the invention are described below with reference to example applications for illustration. It should be understood that numerous specific details, relationships, and methods are set forth to provide a full understanding of the invention. One having ordinary skill in the relevant art, however, will readily recognize that the invention can be practiced without one or more of the specific details or with other methods. In other

instances, well-known structures or operations are not shown in detail to avoid obscuring the invention. The present invention is not limited by the illustrated ordering of acts or events, as some acts may occur in different orders and/or concurrently with other acts or events. Furthermore, not all illustrated acts or events are required to implement a methodology in accordance with the present invention.

Embodiments of the present invention provide methods for determining a reference signal at any location along a transmission media. The methods generally involve sensing at a first location along the transmission media a first signal propagated over the transmission media in a forward direction and a second signal propagated over the transmission media in a reverse direction opposed from the forward direction. The second signal is a reflected version of the first signal. The methods also involve determining a sum signal by adding the first and second signals together and a difference signal by subtracting the second signal from the first signal. A first exponentiation signal is computed using the sum signal. Similarly, a second exponentiation signal is determined using the difference signal. The first exponentiation signal is subtracted from the second exponentiation signal to obtain a reference signal. Notably, the reference signal is defined by a mathematical equation that is not dependant on “z”, the location along the transmission media. As such, the reference signal can be determined at any location along the transmission media and/or at multiple different locations along the transmission media. The reference signal will exhibit the same phase at all locations. Notably, the reference signal(s) can be used in a variety of applications. For example, the reference signal(s) can be used to adjust a phase of transmit and/or receive signals so as to counteract the environmental effects on hardware components of a communication system.

Before describing the systems and methods of the present invention, it will be helpful in understanding exemplary environments in which the invention can be utilized. In this regard, it should be understood that the methods of the present invention can be utilized in a variety of different applications where a reference signal needs to be determined at any location along a transmission media. Such applications include, but are not limited to, mobile/cellular telephone applications, military communication applications, space communication applications, phased array calibration and timing applications, radar signal distribution applications, radar calibration applications for large radar arrays, radar calibration applications for cooperative radar installations, time synchronization applications for sensors, time synchronization applications for digital systems, time synchronization applications for clocks, time synchronization applications for events, and large area (e.g., from several meters to interplanetary) metrology applications.

The word “exemplary” is used herein to mean serving as an example, instance, or illustration. Any aspect or design described herein as “exemplary” is not necessarily to be construed as preferred or advantageous over other aspects or designs. Rather, use of the word exemplary is intended to present concepts in a concrete fashion. As used in this application, the term “or” is intended to mean an inclusive “or” rather than an exclusive “or”. That is, unless specified otherwise, or clear from context, “X employs A or B” is intended to mean any of the natural inclusive permutations. That is if, X employs A; X employs B; or X employs both A and B, then “X employs A or B” is satisfied under any of the foregoing instances.

Systems and Methods for Determining One or More Reference Signals

Referring now to FIG. 1, there is provided a block diagram of a system **100** that is useful for understanding the present invention. As shown in FIG. 1, the system **100** can comprise a signal source **102**, a sensor **116**, a reflective termination **114**, and a non-reflective termination **104**. Each of these components **102**, **104**, **114**, **116** is well known to those having ordinary skill in the art, and therefore will not be described in detail herein. However it should be understood that in order to determine a reference signal V_{ref} , a forward propagated signal V_f and a reverse propagated signal V_r need to be sensed at a location “z” along the transmission media **108**. Although, the transmission media **108** is shown in FIG. 1 to include a coaxial transmission line, embodiments of the present invention are not limited in this regard. For example, the transmission media **108** can also include free space, a waveguide, an optical fiber, and an acoustic media.

In operation, the signal source **102** generally communicates a signal V_f to the reflective termination **114**. A reflected version of the transmitted signal V_r is communicated from the reflective termination **114** to the non-reflective termination **104**. The sensor **116** senses the presence of the forward propagated signal V_f and the reverse propagated signal V_r on the transmission media **108**. The sensor **116** may also adjust the gain of the signals V_f , V_r so that they have equal arbitrarily defined amplitudes “a”. This gain adjustment can involve performing Automatic Gain Control (AGC) operations which are well known to those having ordinary skill in the art. Thereafter, the sensor **116** outputs signals representing the forward propagated signal V_f and the reverse propagated signal V_r . These output signals can subsequently be used to determine the reference signal V_{ref} .

A conceptual diagram of a first exemplary process **200** for determining the reference signal V_{ref} is provided in FIG. 2. As shown in FIG. 2, the process **200** begins by (**202**, **204**) sensing a forward propagated signal V_f and a reverse propagated signal V_r . It should be appreciated that the sensing processes (**202**, **204**) can involve gain adjustments as necessary so that the resulting signals have an arbitrarily defined amplitude a. The gain adjustments can include AGC operations. The forward propagated signal V_f can be defined by the following mathematical equation (1). Similarly, the reverse propagated signal V_r , for the exemplary case of a short circuit reflection, can be defined by the following mathematical equation (2).

$$V_f = a e^{j(\omega t + \phi - \beta z)} \quad (1)$$

$$V_r = -a e^{j(\omega t + \phi + \beta z)} \quad (2)$$

where a is a signal amplitude, j is the square root of minus one ($j = (-1)^{1/2}$), ω is a radian frequency, ϕ is a phase angle, β is a wave number that is equal to $2\pi/\lambda$, where λ is a wavelength. z is a location along a transmission media measured from the reflective end of the transmission media.

Thereafter, a signal combination operation **206** is performed where the signals V_f , V_r are combined to obtain a Sum signal (S). This signal combination operation **206** generally involves adding the signals V_f , V_r together. The signal combination operation **206** can be defined by the following mathematical equation (3).

$$S = a e^{j(\omega t + \phi - \beta z)} - a e^{j(\omega t + \phi + \beta z)} = 2a j e^{j(\omega t + \phi)} [\sin(\beta z)] \quad (3)$$

As evident from mathematical equation (3), the Sum signal S is a signal that depends on the location “z” at which the sensor **116** is placed along the transmission media **108**.

The process **200** also involves performing a subtraction operation **208**. The subtraction operation **208** generally

5

involves subtracting the reverse propagated signal V_r from the forward propagated signal V_f to obtain a Difference signal (D). The subtraction operation **208** can be defined by the following mathematical equation (4).

$$D = ae^{j(\omega t + \phi - z)} + ae^{j(\omega t + \phi + \beta z)} = 2ae^{j(\omega t + \phi)}[\cos(\beta z)] \quad (4)$$

As evident from mathematical equation (4), the Difference signal D is a signal that depends on the location “z” at which the sensor **116** is placed along the transmission media **108**.

After determining the Sum signal S and the Difference signal D, the process **200** continues with a plurality of multiplication operations **210**, **212**. A first one of the multiplication operations **210** generally involves multiplying the Sum signal S by itself to obtain a first Exponentiation signal E_S . The first multiplication operation **210** can generally be defined by the following mathematical equation (5).

$$E_S = S \cdot S = S^2 \quad (5)$$

where E_S is the first Exponentiation signal. S is the Sum signal. S^2 is the Sum signal S raised to the second power.

A second one of the multiplication operations **212** generally involves multiplying the Difference signal D by itself to obtain a second Exponentiation signal E_D . The second multiplication operation **212** can generally be defined by the following mathematical equation (6).

$$E_D = D \cdot D = D^2 \quad (6)$$

where E_D is the second Exponentiation signal. D is the Difference signal. D^2 is the Difference signal D raised to the second power.

Subsequent to determining the first and second Exponentiation signals, the process continues with a subtraction operation **214**. The subtraction operation **214** generally involves subtracting the first Exponentiation signal E_S from the second Exponentiation signal E_D . The subtraction operation **214** can be defined by the following mathematical equation (7).

$$V_{doubled} = D^2 - S^2 = 4a^2 e^{j2(\omega t + \phi)} [\sin^2(\beta z) + \cos^2(\beta z)] = 4a^2 e^{j2(\omega t + \phi)} \quad (7)$$

where $V_{doubled}$ represents a signal obtained as a result of performing the subtraction operation **214**. As evident from mathematical equation (7), the resulting signal $V_{doubled}$ does not depend on the location “z” at which the sensor **116** is placed along the transmission media **108**. As such, the signal $V_{doubled}$ can be determined at one or more locations along a transmission media. This location “z” independence is a significant and highly desirable result.

The resulting signal $V_{doubled}$ has twice the frequency relative to that of each propagated signal V_f , V_r . As such, the resulting signal $V_{doubled}$ can be further processed to increase its frequency to a desired value or to reduce its frequency to a desired value (e.g., the value of the frequency of a propagated signal V_f , V_r). If the resulting signal $V_{doubled}$ is further processed to increase its frequency, then the process **200** can include a multiplication operation (not shown). If the resulting signal $V_{doubled}$ is further processed to reduce its frequency, then the process **200** can include a frequency reduction operation **216**.

The optional frequency reduction operation **216** can generally involve performing a phase locked loop operation and a frequency division operation. Phase locked loop operations are well known to those having ordinary skill in the art, and therefore will not be described herein. The frequency division operation can involve dividing the frequency of the resulting signal $V_{doubled}$ by two (2). The output signal from the fre-

6

quency reduction operation is the reference signal V_{ref} . The reference signal V_{ref} can be defined by the following mathematical equation (8):

$$V_{ref} = \pm e^{j(\omega t + \phi)} \quad (8)$$

for any line position “z”. As evident from mathematical equation (8), the reference signal V_{ref} is a signal that does not depend on the location “z” at which the sensor **116** is placed along the transmission media **108**. As such, the reference signal V_{ref} can be determined at one or more locations along a transmission media. This location “z” independence is a significant and highly desirable result.

Embodiments of the present invention are not limited to the process **200** described above in relation to FIG. **2**. For example, if the frequency of each propagated signal V_f , V_r is reduced by exactly half, then the optional frequency reduction operation **216** need not be performed. A conceptual diagram of a process **300** for determining the reference signal V_{ref} absent of the frequency reduction operation **216** is provided in FIG. **3**. As shown in FIG. **3**, the propagated signals with half the frequency of the signals V_f , V_r have the following designations V'_f , V'_r , respectively.

As shown in FIG. **3**, the process **300** generally involves performing sensing operations **302**, **304** to sense propagated signals V'_f , V'_r , a signal combination operation **306**, subtraction operations **308**, **314**, and multiplication operations **310**, **312**. These listed operations **302**, **304**, . . . , **314** are the same as or substantially similar to the operations **202**, **204**, . . . , **214** of FIG. **2**, respectively. As such, the operations **302**, **304**, . . . , **314** of process **300** will not be described herein.

Referring now to FIG. **4**, there is provided a block diagram of an exemplary system **400** implementing a method for determining a signal $V_{doubled}$ and/or a reference signal V_{ref} . As shown in FIG. **4**, the system **400** comprises a sensing device **402** and a reference signal generator **450**. The reference signal generator **450** includes a signal adder **406**, signal subtractors **408**, **414**, and signal multipliers **410**, **412**. The reference signal generator **450** can also comprise an optional phase lock loop **416** and an optional frequency divider **418**.

The sensing device **402** is generally configured for sensing the presence of a forward propagated signal V_f or V'_f and a reverse propagated signal V_r or V'_r on the transmission media **108**. The sensing device **402** may also adjust the gain of the signals V_f or V'_f , V_r or V'_r , so that they have equal arbitrarily defined amplitudes “a”. This gain adjustment can involve performing AGC operations. The sensing device **402** can also generate output signals representing the forward propagated signal V_f or V'_f and the reverse propagated signal V_r or V'_r . These output signals can subsequently be used to determine the signal $V_{doubled}$ or the reference signal V_{ref} . As such, the sensing device **402** can further communicate the signals representing the forward propagated signal V_f or V'_f and the reverse propagated signal V_r or V'_r to the following components **406**, **408**.

The signal adder **406** is generally configured for performing a signal combination operation **206**, **306** (described above in relation to FIGS. **2** and **3**) to obtain a Sum signal S or S'. The signal subtractor **408** is generally configured for performing a subtraction operation **208**, **308** (described above in relation to FIGS. **2** and **3**) to obtain a Difference signal D or D'. The output signals of the components **406**, **408** are forwarded to the signal multipliers **410**, **412**. Each of the multipliers **410**, **412** is configured to perform a multiplication operation **210**, **212**, **310**, **312** (described above in relation to FIGS. **2** and **3**) to obtain a respective Exponentiation signal E_S , E'_S , E_D , or E'_D . The Exponentiation signals E_S and E_D or E'_S and E'_D are then communicated from the signal multipliers **410**, **412** to

the signal subtractor **414**. At the signal subtractor **414**, a subtraction operation **214**, **314** (described above in relation to FIGS. **2** and **3**) is performed to obtain a signal $V_{doubled}$ or a reference signal V_{ref} .

If the result of the subtraction operation is the signal $V_{doubled}$, then the signal $V_{doubled}$ can be further processed to increase or reduce the value of its frequency. If the frequency of the signal $V_{doubled}$ is to be increased, then the signal $V_{doubled}$ can be forwarded to a multiplier (not shown). If the frequency of the signal $V_{doubled}$ is to be reduced, then the signal $V_{doubled}$ can be forwarded to an optional phase lock loop **416** and an optional frequency divider **418**. The components **416**, **418** collectively act to reduce the frequency of the signal $V_{doubled}$ to a desired value (i.e., the value of the frequency of a propagated signal V_f , V_r). The output of the frequency divider **418** is the reference signal V_{ref} .

Referring now to FIG. **5**, there is provided a block diagram of another exemplary embodiment of a system **500** implementing a method for determining a reference signal V_{ref} . As shown in FIG. **5**, the system **500** comprises a sensing device **504** disposed along a transmission media **502**. Although, the transmission media **502** is shown in FIG. **5** to include a coaxial transmission line, embodiments of the present invention are not limited in this regard. For example, the transmission media **502** can also include free space, a waveguide, and an acoustic media. The system **500** also comprises a reference signal generator **550** for generating a reference signal. Accordingly, the reference signal generator **550** includes a sum-diff hybrid circuit **508**, multipliers **510**, **512**, a signal subtractor **514**, a phase lock loop (PLL) **516**, and a frequency divider **518**. Embodiments of the present invention are not limited to the configuration shown in FIG. **5**. For example, the reference signal generator **550** can be absent of the PLL **516** and the frequency divider **518**. The reference signal generator **550** can also include a phase locked oscillator (not shown) instead of the PLL **516** and the frequency divider **518**.

The sensing device **504** is generally configured for sensing the presence of a forward propagated signal V_f and a reverse propagated signal V_r on the transmission media **502**. The sensing device **504** may also adjust the gain of the signals V_f , V_r so that they have equal arbitrarily defined amplitudes "a". This gain adjustment can involve performing AGC operations. The sensing device **504** can also generate output signals representing the forward propagated signal V_f and the reverse propagated signal V_r . These output signals can subsequently be used to determine the reference signal V_{ref} . As such, the sensing device **504** can further communicate the signals representing the forward propagated signal V_f and the reverse propagated signal V_r to the sum-diff hybrid circuit **508**.

The sum-diff hybrid circuit **508** is generally configured for performing a signal combination operation **206** (described above in relation to FIG. **2**) to obtain a Sum signal S and a subtraction operation **208** (described above in relation to FIG. **2**) to obtain a Difference signal D. Subsequent to completing the signal combination operation **206** and the subtraction operation **208**, the sum-diff hybrid circuit **508** communicates the signals S, D to the multipliers **510**, **512**, respectively. Each of the multipliers **510**, **512** is configured to perform a multiplication operation **210**, **212** (described above in relation to FIG. **2**) to obtain a respective Exponentiation signal E_S , E_D . The Exponentiation signals E_S , E_D are then communicated from the multipliers **510**, **512** to the signal subtractor **514**. At the signal subtractor **514**, a subtraction operation **214** (described above in relation to FIG. **2**) is performed to obtain a signal $V_{doubled}$. The signal $V_{doubled}$ is then processed by the PLL **516** and frequency divider **518** to reduce the frequency of the signal $V_{doubled}$ to a desired value (i.e., the value of the

frequency of a propagated signal V_f , V_r). The output of the frequency divider **518** is the reference signal V_{ref} . It should be noted that the functions of the PLL **516** and the frequency divider **518** can alternatively be performed by a phase locked oscillator (not shown).

Referring now to FIG. **6**, there is provided a block diagram of an exemplary system **600** configured for determining a reference signal V_{REF} when a termination is moving. In order to determine a reference signal V_{REF} , a transmit signal and a reflected signal need to be sensed at a location "Z" along the transmission media. Although the transmission media is shown in FIG. **6** to include free space, embodiments of the present invention are not limited in this regard.

As shown in FIG. **6**, the system **600** comprises a signal source **602**, a moving reflective termination **622**, and a non-reflective termination **604**. Each of these components **602**, **622**, **604** is well known to those having ordinary skill in the art, and therefore will not be described in detail herein. However, it should be appreciated that the signal source **602** can include, but is not limited to, an element control system, Radio Frequency (RF) equipment, and an antenna element. Similarly, the non-reflective termination **604** can include, but is not limited to, an element control system, Radio Frequency (RF) equipment, and an antenna element. The moving reflective termination **622** can be, but is not limited to, an aircraft, a spacecraft, a natural or artificial satellite, or a celestial object (e.g., a planet, a moon, an asteroid, a comet, etc . . .).

In operation, the signal source **602** generally transmits a signal V_{fwd} in the direction **618** of the moving reflective termination **622**. The transmit signal V_{fwd} is the same as the forward propagated signal V_f . As such, the transmit signal V_{fwd} can generally be defined by mathematical equation (1). A reflected version of the transmitted signal V_{rev} is communicated from the moving reflective termination **622** in the direction **620** of the non-reflective termination **604**. The reflected signal V_{rev} can generally be defined by the following mathematical equation (9).

$$V_{rev} = -ae^{j(\omega t + 2\omega_d t + \phi + \beta z)} \quad (9)$$

where ϕ_d is a Doppler frequency shift. The signals V_{fwd} , V_{rev} can be sensed at a location "Z" along the transmission media and subsequently used in a source reference frame (SRF) based process to a determine the reference signal V_{REF} .

The SRF based process is substantially similar to the process described above in relation to FIG. **2**. Accordingly, the SRF based process generally involves performing an addition operation, subtraction operations, and multiplication operations. The addition operation of the SRF based process can generally be defined by the following mathematical equation (10).

$$\text{Sum} = ae^{j(\omega t + \phi - \beta z)} - ae^{j(\omega t + 2\omega_d t + \phi + \beta z)} = 2ae^{j(\omega t + \omega_d t + \phi)} [\sin(\omega_d t + \beta z)] \quad (10)$$

where Sum is a resulting signal of the addition operation of the SRF based process

A first subtraction operation of the SRF based process can generally be defined by the following mathematical equation (11).

$$\text{Diff} = ae^{j(\omega t + \phi - \beta z)} + ae^{j(\omega t + 2\omega_d t + \phi + \beta z)} = 2ae^{j(\omega t + \omega_d t + \phi)} [\cos(\omega_d t + \beta z)] \quad (11)$$

where Diff is a resulting signal of the subtraction operation of the SRF based process.

The multiplication operations of the SRF based process can generally be defined by the following mathematical equations (12) and (13).

$$EX'_S = \text{Sum}^2 \quad (12)$$

$$EX'_D = \text{Diff}^2 \quad (13)$$

where EX'_S and EX'_D are the resulting signals of the multiplication operations of the of the SRF based process.

A second subtraction operation of the SRF based signal sampling process can generally be defined by the following mathematical equation (14).

$$V_{DBL} = \text{Diff}^2 - \text{Sum}^2 = 4a^2 e^{j2(\omega t + \omega_d t + \phi)} [\cos^2(\omega_d t + \beta z) + \sin^2(\omega_d t + \beta z)] - 4a^2 e^{j2(\omega t + \omega_d t + \phi)} \quad (14)$$

where V_{DBL} is a resulting signal of the second subtraction operation of the SRF based process.

Subsequent to determining the signal V_{DBL} , further processing can be performed for increasing or decreasing the signals V_{DBL} frequency. If the frequency of the signal V_{DBL} is reduced by half, then the resulting reference signal V_{REF} can generally be defined by the following mathematical equation (15).

$$V_{REF} = \pm e^{j(\omega t + \omega_d t + \phi)} \quad (15)$$

where V_{REF} is the signal resulting from an optional frequency decrease process of the SRF based process. The optional frequency decrease process can involve performing a phase locked loop operation and a frequency division operation.

Notably, the reference signal V_{REF} can also be determined by performing a moving reference frame (MRF) based process. The MRF based process is substantially similar to the process described above in relation to the SRF based process. Accordingly, the MRF based process generally involves performing an addition operation, subtraction operations, and multiplication operations. However, the transmit signal utilized in the MRF based process is defined by the following mathematical equation (16).

$$V'_{fwd} = a e^{j(\omega t + \omega_d t + \phi - \beta z)} \quad (16)$$

The reverse signal utilized in the MRF signal sampling process is defined by the following mathematical equation (17).

$$V'_{rev} = -a e^{j(\omega t + \omega_d t + \phi + \beta z)} \quad (17)$$

where ω_d is a Doppler frequency shift.

The addition operation of the MRF based process can generally be defined by the following mathematical equation (18).

$$\text{Sum}' = V'_{fwd} + V'_{rev} = a e^{j(\omega t + \omega_d t + \phi - \beta z)} - a e^{j(\omega t + \omega_d t + \phi + \beta z)} = -2a j e^{j(\omega t + \omega_d t + \phi)} [\sin(\beta z)] \quad (18)$$

where Sum' is a resulting signal of the addition operation of the MRF based process.

A first subtraction operation of the MRF based process can generally be defined by the following mathematical equation (19).

$$\text{Diff}' = V'_{fwd} - V'_{rev} = a e^{j(\omega t + \omega_d t + \phi - \beta z)} + a e^{j(\omega t + \omega_d t + \phi + \beta z)} = 2a e^{j(\omega t + \omega_d t + \phi)} [\cos(\beta z)] \quad (19)$$

where Diff' is a resulting signal of the subtraction operation of the MRF based process.

The multiplication operations of the MRF based process can generally be defined by the following mathematical equations (20) and (21).

$$EX'_S = \text{Sum}'^2 \quad (20)$$

$$EX'_D = \text{Diff}'^2 \quad (21)$$

where EX'_S and EX'_D are the resulting signals of the multiplication operations of the MRF based process.

A second subtraction operation of the MRF based process can generally be defined by the following mathematical equation (22).

$$V'_{DBL} = \text{Diff}'^2 - \text{Sum}'^2 = 4a^2 e^{j2(\omega t + \omega_d t + \phi)} [\cos^2(\beta z) + \sin^2(\beta z)] - 4a^2 e^{j2(\omega t + \omega_d t + \phi)} \quad (22)$$

where V'_{DBL} is a resulting signal of the second subtraction operation of the MRF based process. Subsequent to determining the signal V'_{DBL} , further processing can be performed for increasing or decreasing its frequency. If the frequency of the signal is reduced by half, then the resulting signal of the MRF based process is the reference signal V_{REF} .

Referring now to FIG. 7, there is provided a block diagram of an exemplary system 700 that is configured for determining a reference signal when an intermediary device is moving. In order to determine a reference signal V_{ref} , a transmit signal and a reflected signal need to be sensed at a location "z" along the transmission media. Although the transmission media is shown in FIG. 7 to include free space, embodiments of the present invention are not limited in this regard.

As shown in FIG. 7, the system 700 comprises a signal source 702, a reflective termination 722, a moving intermediary device 750, and a non-reflective termination 704. Each of these components 702, 704, 722, 750 is well known to those having ordinary skill in the art, and therefore will not be described in detail herein. However, it should be appreciated that the signal source 702 can include, but is not limited to, an element control system, Radio Frequency (RF) equipment, and an antenna element. Similarly, the non-reflective termination 704 can include, but is not limited to, an element control system, Radio Frequency (RF) equipment, and an antenna element. The reflective termination 722 can be, but is not limited to, a natural satellite, an artificial satellite, and a celestial object (e.g., a planet, a moon, an asteroid, a comet, etc . . .). The moving intermediary device 750 can be, but is not limited to, an aircraft, a space craft, a natural satellite, an artificial satellite, and a celestial object (e.g., a planet, a moon, an asteroid, a comet, etc . . .).

In operation, the signal source 702 generally transmits a signal $V_{forward}$ in the direction 718 of the reflective termination 722. The transmit signal $V_{forward}$ can generally be defined by the following mathematical equation (23).

$$V_{forward} = a e^{j(\omega t + \omega_d t + \phi - \beta z)} \quad (23)$$

where ω_d is a Doppler frequency shift. A reflected version of the transmit signal $V_{reverse}$ is communicated from the reflective termination 722 in the direction 720 of the non-reflective termination 704. The reflected signal $V_{reverse}$ can generally be defined by the following mathematical equation (24).

$$V_{reverse} = -a e^{j(\omega t + \omega_d t + \phi + \beta z)} \quad (24)$$

The signals $V_{forward}$, $V_{reverse}$ can be sensed at a location "z" along the transmission media and subsequently used in an intermediate moving reference frame (IMRF) based process to a determine the reference signal V_{ref} .

The IMRF based process is substantially similar to the process described above in relation to FIG. 2. Accordingly, the IMRF based process generally involves performing an addition operation, subtraction operations, and multiplication operations. The addition operation of the IMRF based process can generally be defined by the following mathematical equation (25).

$$SM = a e^{j(\omega t + \omega_d t + \phi - \beta z)} - a e^{j(\omega t + \omega_d t + \phi + \beta z)} = -2a j e^{j(\omega t + \omega_d t + \phi)} [\sin(\omega_d t + \beta z)] \quad (25)$$

where SM is a resulting signal of the addition operation of the IMRF based process.

11

A first subtraction operation of the IMRF based process can generally be defined by the following mathematical equation (26).

$$\text{DIF} = \frac{ae^{j(\omega t + \omega_d t + \phi - \beta z)} + ae^{j(\omega t + \omega_d t + \phi + \beta z)}}{[\cos(\omega_d t + \beta z)]} = 2ae^{j(\omega t + \omega_d t + \phi)} \quad (26)$$

where DIF is a resulting signal of the subtraction operation of the IMRF based process.

Subsequent to completing the addition and first subtraction operation, the multiplication operations are performed. The multiplication operations of the IMRF based process can generally be defined by the following mathematical equations (27) and (28).

$$\text{ES}_S = \text{SM}^2 \quad (27)$$

$$\text{ED}_D = \text{DIF}^2 \quad (28)$$

where ES_S and ED_D are the resulting signals of the multiplication operations of the IMRF based process.

Once ES_S and ED_D are determined, then a second subtraction operation is performed. The second subtraction operation of the IMRF based process can generally be defined by the following mathematical equation (29).

$$\text{V}_{DB} = \text{DIF}^2 - \text{SM}^2 = 4a^2 e^{j2(\omega t + \omega_d t + \phi)} [\cos^2(\omega_d t + \beta z) + \sin^2(\omega_d t + \beta z)] = 4a^2 e^{j2(\omega t + \omega_d t + \phi)} \quad (29)$$

where V_{DB} is a resulting signal of the second subtraction operation of the IMRF based process. Subsequent to determining the signal V_{DB} , further processing can be performed for increasing or decreasing the signals V_{DB} frequency. If the frequency of the signal V_{DB} is reduced by half, then the resulting signal of the IMRF based process is the reference signal V_{ref} .

It should be noted that a transmit signal generated by the signal source 702 can be stronger than a reflected version of the transmit signal received at the non-reflective termination 704. As a result, coupling of the signals can occur making it difficult to distinguish the signals from each other. In order to resolve this signal coupling issue, the signal source 702 and the non-reflective termination 704 can be spaced apart (e.g., a few hundred yards). Alternatively or additionally, the reflective termination 722 can derive a frequency offset of a transit signal, adjust the frequency thereof utilizing the frequency offset, and communicating a reflected version of the transmit signal with the adjusted frequency to the non-reflective termination 704.

Communication System Including a Reference Signal Generator

FIG. 8 shows an exemplary communication system 800 implementing the present invention. As shown in FIG. 8, the communication system 800 comprises a multi-element antenna system (MEAS) 850 for transmitting signals to and receiving signals from at least one object of interest 808 remotely located from the MEAS 850. In FIG. 8, the object of interest 808 is shown as an airborne or spaceborne object, such as an aircraft, a spacecraft, a natural or artificial satellite, or a celestial object (e.g., a planet, a moon, an asteroid, a comet, etc. . . .). However, embodiments of the present invention are not limited in this regard. The MEAS 850 can also be used for transmitting and receiving signals from objects of interest 808 that are not airborne or spaceborne but are still remotely located with respect to MEAS 850. For example, a ground-based MEAS 850 can be used to provide communications with objects of interest 808 at other ground-based or sea-based locations. The MEAS 850 can generally include an array control system (ACS) 802 for controlling the operation of multiple antenna elements 806a, 806b, 806c.

12

In FIG. 8, the ACS 802 is shown as controlling the operation of antenna elements 806a, 806b, 806c and associated RF equipment 804a, 804b, 804c. The antenna elements 806a, 806b, 806c provide wireless communications. For example, if the MEAS 850 is in a transmit mode, then each antenna element 806a, 806b, 806c converts electrical signals into electromagnetic waves. The radiation pattern 811 resulting from the interference of the electromagnetic waves transmitted by the different antenna elements 806a, 806b, 806c can then be adjusted to a central beam 812 in the radiation pattern 811 aimed in the direction 816 of the object of interest 808. The radiation pattern 811 of the antenna elements 806a, 806b, 806c also generates smaller side beams (or side lobes) 814 pointing in other directions with respect to the direction of the central beam 812. However, because of the relative difference in magnitude between the side beams 814 and the central beam 812, the radiation pattern 811 preferentially transmits the signal in the direction of the central beam 812. Therefore, by varying the phases and the amplitudes of the signals transmitted by each antenna element 806a, 806b, 806c, the magnitude and direction of the central beam 812 can be adjusted. If the MEAS 850 is in a receive mode, then each of the antenna elements 806a, 806b, 806c captures energy from passing waves propagated over transmission media (not shown) in the direction 820 and converts the captured energy to electrical signals. In the receive mode, the MEAS 850 can be configured to combine the electrical signals according to the radiation pattern 811 to improve reception from direction 820, as described below.

In FIG. 8, the antenna elements 806a, 806b, 806c are shown as reflector-type (e.g., a dish) antenna elements, which generally allow adjustment of azimuth (or rotation) and elevation (angle with respect to a ground plane). Therefore, in addition to adjustment of phase and amplitude of the signal transmitted by each of the antenna elements 806a, 806b, 806c, the azimuth and elevation of each antenna element 806a, 806b, 806c can also be used to further steer the central beam 812 and adjust the radiation pattern 811. However, embodiments of the present invention are not limited on this regard. The antenna elements 806a, 806b, 806c can comprise directional or omni-directional antenna elements.

Although three (3) antenna elements 806a, 806b, 806c are shown in FIG. 8, the various embodiments of the present invention are not limited in this regard. Any number of antenna elements 806a, 806b, 806c can be used without limitation. Furthermore, the spacing between the antenna elements 806a, 806b, 806c with respect to each other is not limited. Accordingly, the antenna elements 806a, 806b, 806c can be widely spaced or closely spaced. However, as the spacing between the antenna elements 806a, 806b, 806c increases, the central beam 812 generally becomes narrower and the side beams (or side lobes) 814 generally become larger. The antenna elements 806a, 806b, 806c can also be regularly spaced (not shown) with respect to one another or arbitrarily spaced (or non-linearly spaced) with respect to one another (as shown in FIG. 8) to form a three dimensional (3D) array of antenna elements. As shown in FIG. 8, the arbitrary spacing of the antenna elements 806a, 806b, 806c can include locations having different altitudes and locations having different distances between each other.

As shown in FIG. 8, each of the antenna elements 806a, 806b, 806c is communicatively coupled to a respective RF equipment 804a, 804b, 804c via a respective cable assembly 810a, 810b, 810c (collectively 810). Each of the cable assemblies 810a, 810b, 810c can have the same or different lengths. As used herein, the phrase "cable assemblies" refers to any number of cables provided or interconnecting two different

components. In the various embodiments of the present invention, the cables in the cable assemblies **810a**, **810b**, **810c** can be bundled or unbundled.

Notably, the cables **810a**, **810b**, **810c** can delay transmit signals. In effect, the phases of the transmit signals can be shifted thereby resulting in phasing errors. As such, the communication system **800** implements a closed loop method to counteract phasing errors due to cable delay effects. The closed loop method will become more evident as the discussion progresses.

The RF equipment **804a**, **804b**, **804c** control the antenna elements **806a**, **806b**, **806c**, respectively. For example, for the directional antenna elements **806a**, **806b**, **806c** shown in FIG. **8**, the RF equipment **804a**, **804b**, **804c** can be configured to control antenna motors (not shown), antenna servo motors (not shown), and antenna rotators (not shown). The RF equipment **804a**, **804b**, **804c** can also include hardware entities for processing transmit signals and receive signals. Notably, the phases of transmit signals can be shifted as a result of environmental effects on the cabling, antenna, and/or RF equipment **804a**, **804b**, **804c**. These phase shifts can result in the steering of the radiated central beam **812** in a direction other than the direction **816** of the object of interest **808**. The RF equipment **804a**, **804b**, **804c** will be described in more detail below in relation to FIG. **9**.

As shown in FIG. **8**, each of the RF equipment **804a**, **804b**, **804c** is communicatively coupled to the ACS **802** via a respective communications link **818a**, **818b**, **818c**. Generally, such communications links are provided via a cable assembly. However, embodiments of the present invention are not limited in this regard. In the various embodiments of the present invention, the communications links **818a**, **818b**, **818c** can comprise wireline, optical, or wireless communication links. The cable assemblies for the communications links **818a**, **818b**, **818c** can have the same or different lengths. Although the communications links **818a**, **818b**, **818c** are shown to couple the RF equipment **804a**, **804b**, **804c** to the ACS **802** in parallel, embodiments of the present invention are not limited in this regard. The RF equipment **804a**, **804b**, **804c** can also be coupled to the ACS **802** in a series arrangement, such as that shown by communication links **819a**, **819b**, **819c**.

Notably, the cable assemblies of the communication links **818a**, **818b**, **818c**, **819a**, **819b**, **819c** can delay transmit signals. In effect, the phases of the transmit signals can be shifted thereby resulting in phasing errors. Additionally, the RF electronic components **804a**, **804b**, **804c** used in the antennas (such as power amplifiers, filters and feed horns) may also introduce phase errors. All these errors are further subject to changes in phase due to operating environment and signal levels. As such, the communication system **800** implements a closed loop method to counteract phasing errors due to imperfect phase matching. The closed loop method will become more evident as the discussion progresses.

In operation, the ACS **802** modulates signals to be transmitted by the antenna elements **806a**, **806b**, **806c**. The ACS **802** also demodulates signals received from other antenna systems. The ACS **802** further controls beam steering. Notably, the interconnecting cables, antenna elements **806a**, **806b**, **806c**, and RF equipment **804a**, **804b**, **804c** can be affected by surrounding environmental conditions (e.g., heat). Such phase shifts can result in the steering of the radiated central beam **812** in a direction other than the direction **816** of the object of interest **808**. As such, the communication system **800** implements a closed loop method to counteract phasing errors due to environmental effects on ACS **802**. The closed

loop method will become more evident as the discussion progresses. The ACS **802** will be described in more detail below in relation to FIG. **9**.

In view of the forgoing, it should be appreciated that the cables **810a**, **810b**, **810c** and the communications links **818a**, **818b**, **818c** (or **819a**, **819b**, **819c**) of the communication system **800** delay signals between the ACS **802** and the antenna elements **806a**, **806b**, **806c**. In effect, the phases of the signals are shifted thereby resulting in phasing errors. Such errors are exacerbated by the spacing between the antenna elements **806a**, **806b**, **806c**. Phasing errors further occur as a result of environmental effects on the hardware components **802**, **804a**, **804b**, **804c** of the communication system **800**. The accumulated phasing errors inhibit desirable or adequate beam formation, i.e., the accumulated phasing errors can result in the steering of the radiated central beam **812** in a direction other than the direction **816** of the object of interest **808**.

Accordingly, the communication system **800** is configured to adjust the phases and/or amplitudes of signals transmitted from and received at each antenna element **806a**, **806b**, **806c** so as to counteract the errors in phasing. The phases and/or amplitudes of the transmit and receive signals can be adjusted using a reference signal V_{ref} . This phase and/amplitude adjustment function of the communication system **800** will become more evident as the discussion progresses.

Referring now to FIG. **9**, there is provided a more detailed block diagram of the communication system **800** that is useful for understanding the phase and/or amplitude adjustment function thereof. Notably, the antenna elements **806a**, **806b**, **806c** and RF equipment **804b**, **804c** are not shown in FIG. **9** to simplify the following discussion. However, it should be understood that the antenna elements **806b**, **806c** are the same as or substantially similar to the antenna element **806a**. Similarly, the RF equipment **804b**, **804c** is the same as or substantially similar to the RF equipment **804a**.

As shown in FIG. **9**, the ACS **802** comprises a station frequency reference **903**, a Transmit Radio Signal Generator (TRSG) **904**, hardware entities **906**, beamformers **908**, **935**, a power coupler **913**, a phase/amplitude controller **910**, a phase comparator **912b**, and a reference signal generator **914b**. Embodiments of the present invention are not limited in this regard. For example, the ACS **802** can include a set of components **906**, **908**, **910**, **912b**, **913**, **914b**, and **935** for each antenna element **806a**, **806b**, **806c**. As also shown in FIG. **9**, the RF equipment **804a** comprises hardware entities **942**, a high power amplifier (HPA) **944**, a phase comparator **912a**, and a reference signal generator **914a**. Embodiments of the present invention are not limited in this regard. For example, the RF equipment **804a** can be absent of hardware entities **942**. As also shown in FIG. **9**, the MEAS **850** comprises a $\frac{1}{2}$ transmit carrier frequency device **915**, an analog fiber modulator **917**, an optical fiber **925**, and a fiber mirror **923**.

The TRSG **904** of the ACS **802** can generate signals to be transmitted from the antenna elements **806a**, **806b** (not shown), **806c** (not shown). The TRSG **904** is communicatively coupled to the station frequency reference **903** and the hardware entities **906**. The phrase "hardware entities", as used herein, refers to signal processing devices, including but not limited to, filters and amplifiers. The hardware entities **906** are communicatively coupled to the beamformer **908**.

The beamformers **908** can be utilized to control the phases and/or the amplitudes of transmit signals. In general, the phases and/or amplitudes of the transmit signal can be used to adjust formation of the central beam **812**, the side beams (or side lobes) **814**, and nulls in the radiation pattern **811**. Nulls correspond to directions in which destructive interference

results in a transmit signal's strength that is significantly reduced with respect to the directions of the central beam **812** and the side beams **814**. The beamformer **908** combines a complex weight w_N with transmit signals to be provided to the RF equipment **804a**, **804b** (not shown), **804c** (not shown).

The beamformer **908** is communicatively coupled to power coupler **913**. The power coupler **913** is communicatively coupled to the closed loop operator **998**. The closed loop operator **998** will be described below. However, it should be understood that the closed loop operator **998** is generally configured to adjust the phase and/or amplitude of transmit signals and communicate the phase and/or amplitude adjusted transmit signals to the hardware entities **942** of the RF equipment **804a**. The hardware entities **942** are communicatively coupled to the HPA **944**. HPAs are well known to those having ordinary skill in the art, and therefore will not be described herein. However, it should be understood that the HPA **944** communicates signals to the antenna element **806a** for transmission therefrom.

The closed loop operator **998** is generally configured for controlling the phases and/or amplitudes of transmit signals so as to counteract phasing errors due to cable delay effects, wide antenna spacing effects, and environmental effects on hardware components **802** and **804a** of the communication system **800**. Accordingly, the closed loop operator **998** includes the phase comparators **912a**, **912b**, the phase/amplitude controller **910**, and the beamformer **935**.

The phase comparator **912a** is configured to receive a transmit signal **960** from the antenna element **806a** and a reference signal V_{ref-1} from a reference signal generator **914a**. In this regard, it should be understood that the antenna element **806a** has a transmit (Tx) signal probe **928** disposed thereon for sensing the transmit signal **960**. At the phase comparator **912a**, the phase of the sensed transmit signal **960** is compared with the phase of the reference signal V_{ref-1} to determine a phase offset **970**. The phase offset **970** can be represented in terms of an imaginary part Q and a real part I. The phase offset **970** is then communicated from the phase comparator **912a** to the phase/amplitude controller **910**.

The reference signal V_{ref-1} utilized by the phase comparator **912a** is generated by the reference signal generator **914a**. The reference signal generator **914a** is configured to receive sensed signals V_β , V_r from one or more sensor devices (not shown) disposed on the optical fiber **925** at a first location. Additionally or alternatively, the reference signal generator **914a** is configured to sense signals V_β , V_r propagated along the optical fiber **925**. The sensed signals V_β , V_r are used to determine the reference signal V_{ref-1} . The manner in which the reference signal V_{ref-1} is determined is described above in relation to FIGS. 1-3. The reference signal generator **914a** can be the same as or substantially similar to any one of the reference signal generator shown in FIGS. 4 and 5.

The phase comparator **912b** is configured to receive a transmit signal **950** from the power coupler **913** and a reference signal V_{ref-2} from a reference signal generator **914b**. At the phase comparator **912b**, the phase of the transmit signal **950** is compared with the phase of the reference signal V_{ref-2} to determine a phase offset **916**. The phase offset **916** can be represented in terms of an imaginary part Q and a real part I. The phase offset **916** is then communicated from the phase comparator **912b** to the phase/amplitude controller **910**.

The reference signal V_{ref-2} utilized by the phase comparator **912b** is generated by the reference signal generator **914b**. The reference signal generator **914b** is configured to receive sensed signals V_β , V_r from one or more sensor devices (not shown) disposed on the optical fiber **925** at a second location different from the first location. Additionally or alternatively,

the reference signal generator **914b** is configured to sense signals V_β , V_r propagated along the optical fiber **925**. The sensed signals V_β , V_r are used by the reference signal generator **914b** to determine the reference signal V_{ref-2} . The manner in which the reference signal V_{ref-2} is determined is described above in relation to FIGS. 1-3. The reference signal generator **914b** can be the same as or substantially similar to any one of the reference signal generator shown in FIGS. 4 and 5. The reference signal generator **914b** can also be the same as or substantially similar to the reference signal generator **914a**.

The phase/amplitude controller **910** determines the phase and/or amplitude adjustment value Δw_N that is to be used by the beamformer **935** to adjust the phase and/or amplitude of transmit signals. The phase and/or amplitude adjustment value Δw_N is determined using the received phase offset **916**, **970** values received from the phase comparators **912b**, **912a**, respectively.

FIG. 10 is a schematic diagram of a computer system **1000** for executing a set of instructions that, when executed, can cause the computer system to perform one or more of the methodologies and procedures described above. For example, a computer system **1000** can be implemented to perform the various tasks of the systems **400**, **500**, **600**, **700**, **800**. In some embodiments, the computer system **1000** operates as a single standalone device. In other embodiments, the computer system **1000** can be connected (e.g., using a network) to other computing devices to perform various tasks in a distributed fashion. In a networked deployment, the computer system **1000** can operate in the capacity of a server or a client developer machine in server-client developer network environment, or as a peer machine in a peer-to-peer (or distributed) network environment.

The computer system **1000** can comprise various types of computing systems and devices, including a server computer, a client user computer, a personal computer (PC), a tablet PC, a laptop computer, a desktop computer, a control system, a network router, switch or bridge, or any other device capable of executing a set of instructions (sequential or otherwise) that specifies actions to be taken by that device. It is to be understood that a device of the present disclosure also includes any electronic device that provides voice, video or data communication. Further, while a single computer is illustrated, the phrase "computer system" shall be understood to include any collection of computing devices that individually or jointly execute a set (or multiple sets) of instructions to perform any one or more of the methodologies discussed herein.

The computer system **1000** can include a processor **1002** (such as a central processing unit (CPU), a graphics processing unit (GPU, or both), a main memory **1004** and a static memory **1006**, which communicate with each other via a bus **1008**. The computer system **1000** can further include a display unit **1010**, such as a video display (e.g., a liquid crystal display or LCD), a flat panel, a solid state display, or a cathode ray tube (CRT)). The computer system **1000** can include an input device **1012** (e.g., a keyboard), a cursor control device **1014** (e.g., a mouse), a disk drive unit **1016**, a signal generation device **1018** (e.g., a speaker or remote control) and a network interface device **1020**.

The disk drive unit **1016** can include a computer-readable storage medium **1022** on which is stored one or more sets of instructions **1024** (e.g., software code) configured to implement one or more of the methodologies, procedures, or functions described herein. The instructions **1024** can also reside, completely or at least partially, within the main memory **1004**, the static memory **1006**, and/or within the processor **1002** during execution thereof by the computer system **1000**.

The main memory **1004** and the processor **1002** also can constitute machine-readable media.

Dedicated hardware implementations including, but not limited to, application-specific integrated circuits, programmable logic arrays, and other hardware devices can likewise be constructed to implement the methods described herein. Applications that can include the apparatus and systems of various embodiments broadly include a variety of electronic and computer systems. Some embodiments implement functions in two or more specific interconnected hardware modules or devices with related control and data signals communicated between and through the modules, or as portions of an application-specific integrated circuit. Thus, the exemplary system is applicable to software, firmware, and hardware implementations.

In accordance with various embodiments of the present disclosure, the methods described herein can be stored as software programs in a computer-readable storage medium and can be configured for running on a computer processor. Furthermore, software implementations can include, but are not limited to, distributed processing, component/object distributed processing, parallel processing, virtual machine processing, which can also be constructed to implement the methods described herein.

The present disclosure contemplates a computer-readable storage medium containing instructions **1024** or that receives and executes instructions **1024** from a propagated signal so that a device connected to a network environment **1026** can send or receive voice and/or video data, and that can communicate over the network **1026** using the instructions **1024**. The instructions **1024** can further be transmitted or received over a network **1026** via the network interface device **1020**.

While the computer-readable storage medium **1022** is shown in an exemplary embodiment to be a single storage medium, the term “computer-readable storage medium” should be taken to include a single medium or multiple media (e.g., a centralized or distributed database, and/or associated caches and servers) that store the one or more sets of instructions. The term “computer-readable storage medium” shall also be taken to include any medium that is capable of storing, encoding or carrying a set of instructions for execution by the machine and that cause the machine to perform any one or more of the methodologies of the present disclosure.

The term “computer-readable medium” shall accordingly be taken to include, but not be limited to, solid-state memories such as a memory card or other package that houses one or more read-only (non-volatile) memories, random access memories, or other re-writable (volatile) memories; magneto-optical or optical medium such as a disk or tape; as well as carrier wave signals such as a signal embodying computer instructions in a transmission medium; and/or a digital file attachment to e-mail or other self-contained information archive or set of archives considered to be a distribution medium equivalent to a tangible storage medium. Accordingly, the disclosure is considered to include any one or more of a computer-readable medium or a distribution medium, as listed herein and to include recognized equivalents and successor media, in which the software implementations herein are stored.

Although the present specification describes components and functions implemented in the embodiments with reference to particular standards and protocols, the disclosure is not limited to such standards and protocols. Each of the standards for Internet and other packet switched network transmission (e.g., TCP/IP, UDP/IP, HTML, and HTTP) represent examples of the state of the art. Such standards are periodically superseded by faster or more efficient equiva-

lents having essentially the same functions. Accordingly, replacement standards and protocols having the same functions are considered equivalents.

In light of the forgoing description of the invention, it should be recognized that the present invention can be realized in hardware, software, or a combination of hardware and software. A method for determining a reference signal according to the present invention can be realized in a centralized fashion in one processing system, or in a distributed fashion where different elements are spread across several interconnected processing systems. Any kind of computer system, or other apparatus adapted for carrying out the methods described herein, is suited. A typical combination of hardware and software could be a general purpose computer processor, with a computer program that, when being loaded and executed, controls the computer processor such that it carries out the methods described herein. Of course, an application specific integrated circuit (ASIC), and/or a field programmable gate array (FPGA) could also be used to achieve a similar result.

Applicants present certain theoretical aspects above that are believed to be accurate that appear to explain observations made regarding embodiments of the present invention. However, embodiments of the present invention may be practiced without the theoretical aspects presented. Moreover, the theoretical aspects are presented with the understanding that Applicants do not seek to be bound by the theory presented.

While various embodiments of the present invention have been described above, it should be understood that they have been presented by way of example only, and not limitation. Numerous changes to the disclosed embodiments can be made in accordance with the disclosure herein without departing from the spirit or scope of the invention. Thus, the breadth and scope of the present invention should not be limited by any of the above described embodiments. Rather, the scope of the invention should be defined in accordance with the following claims and their equivalents.

Although the invention has been illustrated and described with respect to one or more implementations, equivalent alterations and modifications will occur to others having ordinary skill in the art upon the reading and understanding of this specification and the annexed drawings. In addition, while a particular feature of the present invention may have been disclosed with respect to only one of several implementations, such feature may be combined with one or more other features of the other implementations as may be desired and advantageous for any given or particular application.

The terminology used herein is for the purpose of describing particular embodiments only and is not intended to be limiting of the invention. As used herein, the singular forms “a”, “an” and “the” are intended to include the plural forms as well, unless the context clearly indicates otherwise. Furthermore, to the extent that the terms “including”, “includes”, “having”, “has”, “with”, or variants thereof are used in either the detailed description and/or the claims, such terms are intended to be inclusive in a manner similar to the term “comprising.”

Unless otherwise defined, all terms (including technical and scientific terms) used herein have the same meaning as commonly understood by one of ordinary skill in the art to which this invention belongs. It will be further understood that terms, such as those defined in commonly used dictionaries, should be interpreted as having a meaning that is consistent with their meaning in the context of the relevant art and will not be interpreted in an idealized or overly formal sense unless expressly so defined herein.

I claim:

1. A method for utilizing at least one reference signal in an antenna system, said reference signal determined at any location along a transmission media, comprising the steps of:

sensing at a first location along the transmission media a first signal propagated over the transmission media in a forward direction and a second signal propagated over the transmission media in a reverse direction opposed from the forward direction, the second signal being a reflected version of the first signal;

adjusting a gain of at least one of the first and second signals so that the first and second signals have equal arbitrarily defined amplitudes;

determining a first sum signal by adding the first and second signals together and a first difference signal by subtracting the second signal from the first signal;

determining a first exponentiation signal by raising the first sum signal to a second power and a second exponentiation signal by raising the first difference signal to the second power;

determining a first reference signal by subtracting the first exponentiation signal from the second exponentiation signal;

performing closed loop operations using the first reference signal to determine at least one weight useful for controlling beam steering of the antenna system; and

controlling beam steering of the antenna system by using the weight to modify a transmit signal, whereby beam steering errors caused by an error in a phase of the transmit signal are counteracted.

2. The method according to claim 1, further comprising increasing or decreasing a first frequency of the first reference signal by a certain amount.

3. The method according to claim 1, wherein the first reference signal has a first frequency different than a second frequency of the first signal.

4. The method according to claim 3, further comprising the step of processing the first reference signal to obtain an adjusted reference signal with a third frequency equal to the second frequency of the first signal.

5. The method according to claim 1, further comprising the steps of:

sensing at a second location different from the first location along the transmission media the first and second signal; and

determining a second reference signal using the first and second signals sensed at the second location; wherein the second reference signal has the same phase as the first reference signal.

6. The method according to claim 5, wherein the step of determining a second reference signal comprises

determining a second sum signal by adding the first and second signals sensed at the second location together and a second difference signal by subtracting the second signal sensed at the second location from the first signal sensed at the second location,

determining a third exponentiation signal by raising the second sum signal to the second power and a fourth exponentiation signal by raising the second difference signal to the second power, and

determining the second reference signal by subtracting the third exponentiation signal from the fourth exponentiation signal.

7. The method according to claim 5, wherein the closed loop operations further comprise using the second reference signal to determine the weight.

8. The method according to claim 5, wherein the closed loop operations further comprise comparing a phase of the transmit signal with a phase of the first reference signal to determine a phase offset.

9. The method according to claim 1, further comprising communicating the first signal from a signal source to a reflective termination over the transmission media, and communicating said second signal from the reflective termination to a non-reflective termination over the transmission media, said reflective termination moving relative signal source.

10. A method for utilizing at least one reference signal in an antenna system, said reference signal determined at any location along a transmission media, comprising the steps of:

sensing at a first location along the transmission media a first signal propagated over the transmission media in a forward direction and a second signal propagated over the transmission media in a reverse direction opposed from the forward direction, the second signal being a reflected version of the first signal;

sensing at a second location different from the first location along the transmission media the first and second signals;

adjusting a gain of at least one of the first and second signals so that the first and second signals have equal arbitrarily defined amplitudes;

determining a first sum signal by adding the first and second signals sensed at the first location together and a first difference signal by subtracting the second signal sensed at the first location from the first signal sensed at the first location;

determining a first exponentiation signal by raising the first sum signal to a second power and a second exponentiation signal by raising the first difference signal to the second power;

determining a first reference signal by subtracting the first exponentiation signal from the second exponentiation signal;

determining a second reference signal using the first and second signals sensed at the second location;

performing closed loop operations using the first reference signal and the second reference signal to determine at least one weight useful for controlling beam steering of the antenna system; and

controlling beam steering of the antenna system by using the weight to modify a transmit signal, whereby beam steering errors caused by an error in a phase of the transmit signal are counteracted; wherein the second reference signal has the same phase as the first reference signal.

11. The method according to claim 10, wherein the first reference signal has a first frequency equal to a second frequency of the first signal.

12. The method according to claim 10, wherein the first reference signal has a first frequency different than a second frequency of the first signal.

13. The method according to claim 12, further comprising the step of processing the first reference signal to obtain an adjusted reference signal with a third frequency equal to the second frequency of the first signal.

14. The method according to claim 10, wherein the step of determining the second reference signal comprises

determining a second sum signal by adding the first and second signals sensed at the second location together and a second difference signal by subtracting the second signal sensed at the second location from the first signal sensed at the second location,

21

determining a third exponentiation signal by raising the second sum signal to the second power and a fourth exponentiation signal by raising the second difference signal to the second power, and

subtracting the third exponentiation signal from the fourth exponentiation signal to obtain the second reference signal.

15 **15.** The method according to claim **14**, further comprises the step of processing the second reference signal to obtain an adjusted reference signal with a first frequency equal to a second frequency of the first signal.

16. A method for utilizing at least one reference signal in an antenna system, said reference signal determined at any location along a transmission media, comprising the steps of:

sensing at a first location along the transmission media a first signal propagated over the transmission media in a forward direction and a second signal propagated over the transmission media in a reverse direction opposed from the forward direction, the second signal being a reflected version of the first signal;

adjusting a gain of at least one of the first and second signals so that the first and second signals have equal arbitrarily defined amplitudes;

determining a first sum signal by adding the first and second signals together and a first difference signal by subtracting the second signal from the first signal;

determining a first exponentiation signal by raising the first sum signal to a second power and a second exponentiation signal by raising the first difference signal to the second power;

22

determining a first reference signal by subtracting the first exponentiation signal from the second exponentiation signal;

performing closed loop operations using the first reference signal to determine at least one weight useful for controlling beam steering of the antenna system; and

using the weight to adjust the phase or amplitude of a communication signal so as to counteract beam steering errors caused by an error in a phase of the communication signal.

10 **17.** The method according to claim **16**, wherein the first reference signal has a first frequency equal to a second frequency of the first signal.

15 **18.** The method according to claim **16**, wherein the first reference signal has a first frequency different than a second frequency of the first signal.

19. The method according to claim **18**, further comprising the step of processing the first reference signal to obtain an adjusted reference signal with a third frequency equal to the second frequency of the first signal.

20 **20.** The method according to claim **18**, further comprising the steps of:

sensing at a second location different from the first location along the transmission media the first and second signal;

and

determining a second reference signal using the first and second signals sensed at the second location;

wherein the second reference signal has the same phase as the first reference signal.

* * * * *